

Sample &

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bq51050B, bq51051B, bq51052B

SLUSB42E - JULY 2012 - REVISED MARCH 2015

# bq5105xB High-Efficiency Qi v1.1-Compliant Wireless Power Receiver and Battery Charger

Technical

Documents

# 1 Features

- Single-Stage Wireless Power Receiver and Li-Ion/Li-Pol Battery Charger
  - Combines Wireless Power Receiver, Rectifier, and Battery Charger in a Single, Small Package
  - 4.20-V, 4.35-V, and 4.40-V Output Voltage Options
  - Supports a Charging Current up to 1.5 A
  - 93% Peak AC-DC Charging Efficiency
- Robust Architecture
  - 20-V Maximum Input Voltage Tolerance, With Input Overvoltage Protection
  - Thermal Shutdown and Overcurrent Protection
  - Temperature Monitoring and Fault Detection
- Compatible With WPC v1.1 Qi Industry Standard
- Power Stage Output Tracks Rectifier and Battery Voltage to Ensure Maximum Efficiency Across the Full Charge Cycle
- Available in Small DSGBA and VQFN Packages

# 2 Applications

- Battery Packs
- Cell Phones and Smart Phones
- Headsets
- Portable Media Players
- Other Handheld Devices

# 3 Description

Tools &

Software

The bq5105x device is a high-efficiency, Qi-compliant wireless power receiver with an integrated Li-Ion/Li-Pol battery charge controller for portable applications. The bq5105xB devices provide efficient AC-DC power conversion, integrates the digital controller required to comply with Qi v1.1 communication protocol, and provides all necessary control algorithms needed for efficient and safe Li-lon and Li-Pol battery charging. Together with the bq500212A transmitter-side controller, the bq5105x enables a complete wireless power transfer system for direct battery charger solutions. By using near-field inductive power transfer, the receiver coil embedded in the portable device can pick up the power transmitted by transmitter coil. The AC signal from the receiver coil is then rectified and conditioned to apply power directly to the battery. Global feedback is established from the receiver to the transmitter to stabilize the power transfer process. This feedback is established by using the Qi v1.1 communication protocol.

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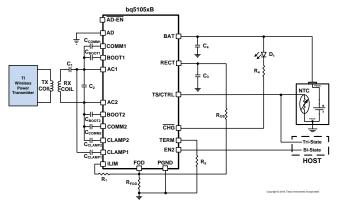
The bq5105xB devices integrate a low-impedance synchronous rectifier, low-dropout regulator (LDO), digital control, charger controller, and accurate voltage and current loops in a single package. The entire power stage (rectifier and LDO) use low-resistance N-MOSFETs (100-m $\Omega$  typical Rdson) to ensure high efficiency and low power dissipation.

_	•••••	-
PART NUMBER	PACKAGE	BODY SIZE (NOM)
bq51050B	VQFN (20)	4.50 mm × 3.50 mm
bq51051B bq51052B	DSBGA (28)	3.00 mm × 1.90 mm

# Device Information<sup>(1)</sup>

(1) For all available packages, see the orderable addendum at the end of the data sheet.

## **Typical Application Schematic**





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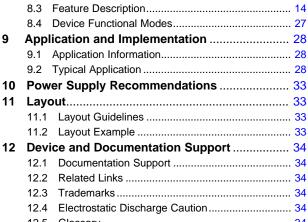
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•	Added ESD Ratings table, Feature Description section, Device Functional Modes, Application and Implementation section, Power Supply Recommendations section, Layout section, Device and Documentation Support section, and Mechanical, Packaging, and Orderable Information section.	1
•	Added the bq51052B 4.40-V option	. 1
•	Updated pinout images	
•	Added thermal pad description in Pin Functions table	
•	Added AD voltage to ROC for clarity	. 6
•	Changed RECT overvoltage specification name from V <sub>RECT</sub> to V <sub>OVP</sub>	. 7
•	Changed to I <sub>LIM_SHORT, OK</sub> from I <sub>LIM_SC</sub> for clarity	
•	Added V <sub>OREG</sub> for bq51052B	
•	Added minimum current for K <sub>ILIM</sub>	. 8
•	Changed Typical value from 300 to 314 (min / max also changed)	. 8
•	Added spec for charging minimum and maximum	. 8
•	Added V <sub>RECH</sub> for bq51052B	
•	Added new spec I <sub>Termination</sub>	
•	Changed to VTSB from VTS for clarity	. 8
•	Changed from I <sub>TS-Bias</sub> for clarity	
•	Deleted V <sub>0C-F</sub> as redundant	
•	Changed typical JEITA regulation on bq51050B from 4.10 V to 4.06 V	. 8
•	Changed to clarify CTRL pin high and low levels	. 8
•	Changed Thermal shutdown name to T <sub>J-SD</sub> for clarity	
•	Added section to describe Adapter Enable function	. 9
•	Changed Synchronous rectifer switchover name to I <sub>BAT-SR</sub> for clarity	. 9
•	Added synchronous mode entry for bq51052B	. 9
•	Deleted note regarding internal junction monitor reducing current - it is not applicable.	19
•	Added section on modified JEITA profile for bq51052B	21



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## **Revision History (continued)**

•	Changed TS/CTRL function to correct Termination Packet value	22
•	Added Taper mode completion for Termination Packet	22
•	Changed Beta value from 4500 to 3380 to match NTC datasheet	25
•	Changed received power maximum error from 250 mW to 375 mW to comply with latest WPC v1.1 specification	26

#### Changes from Revision C (February 2013) to Revision D

•	Changed the ABSOLUTE MAXIMUM RATINGS - moved AC1 and AC2 onto a single row with a Min value of -0.8	6
•	Added section: Details of a Qi Wireless Power System and bq5105xB Power Transfer Flow Diagrams	. 15
•	Changed text in the Battery Charge Profile section	19
•	Changed Battery failure Conditions in Table 1	22
•	Changed Equation 3 and Equation 4	24
•	Changed R <sub>2</sub> = 7.81 k $\Omega$ To: R <sub>1</sub> = 29.402 k $\Omega$	25
•	Changed R <sub>3</sub> = 13.98 k $\Omega$ To: R <sub>3</sub> = 14.302 k $\Omega$	25
•	Changed T <sub>HOT</sub> = 0°C To: T <sub>HOT</sub> = 60°C	25
•	Changed Equation 6	29

#### Changes from Revision B (September 2012) to Revision C

•	First release of the full data sheet	1
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#### Changes from Revision A (August 2012) to Revision B

	Changed last features bullet from: 1.9 x 3.0mm WCSP and 4.5 x 3.5mm QFN Package Options to: Available in small WCSP and QFN packages	. 1
•	Changed Figure 1 and changed caption from: Wireless Power Consortium (WPC or Qi) Inductive Power Charging System, to: Typical System blocks shows bq5105xB used as a Wireless Power Li-Ion/Li-Pol Battery Charger	. 1

#### Changes from Original (August 2012) to Revision A

•	Changed Regulated BAT(output) voltage	. 8
	Changed Recharge threshold for bq51052B	
•	Deleted I <sub>TS-Bias-Max</sub>	. 8
•	Changed V <sub>COLD</sub> to V <sub>OC</sub> and values	. 8
•	Changed V <sub>45C</sub> values	. 8
•	Changed V <sub>60C</sub> values	. 8
•	Changed Figure 25	21
•	Changed Figure 25	22

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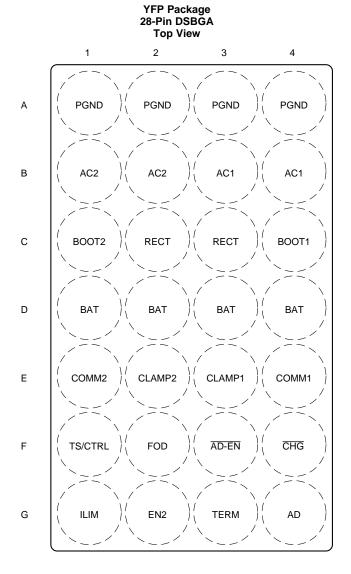
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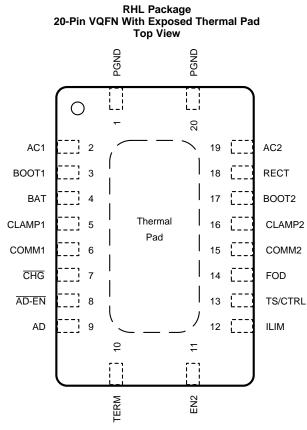
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# 5 Device Options

DEVICE	FUNCTION	V <sub>RECT-OVP</sub>	V <sub>RECT-REG</sub>	V <sub>BAT-REG</sub>	NTC MONITORING
bq51050B	4.20-V Li-Ion Wireless Battery Charger	15 V	Track	4.20 V	JEITA
bq51051B	4.35-V Li-Ion Wireless Battery Charger	15 V	Track	4.35 V	JEITA
bq51052B	4.40-V Li-Ion Wireless Battery Charger	15 V	Track	4.40 V	Modified JEITA

# 6 Pin Configuration and Functions





The exposed thermal pad should be connected to ground.



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#### **Pin Functions**

Pin .						
NAME	DSBGA	VQFN	I/O	DESCRIPTION		
AC1	B3, B4	2	I	Input power from receiver coil.		
AC2	B1, B2	19	I	Input power from receiver coil.		
AD	G4	9	I	If AD functionality is used, connect this pin to the wired adapter input. When $V_{AD-Pres}$ is applied to this pin wireless charging is disabled and AD_ENn is driven low. Connect a 1- $\mu$ F capacitor from AD to PGND. If unused, the capacitor is not required and AD should be connected directly to PGND.		
AD-EN	F3	8	0	Push-pull driver for external PFET when wired charging is active. Float if not used.		
	D1					
DAT	D2		~			
BAT	D3	4	0	Output pin, delivers power to the battery while applying the internal charger profile.		
	D4					
BOOT1	C4	3	0	Bootstrap capacitors for driving the high-side FETs of the synchronous rectifier. Connect a 10-nF		
BOOT2	C1	17	0	ceramic capacitor from BOOT1 to AC1 and from BOOT2 to AC2.		
CHG	F4	7	0	Open-drain output – active when BAT is enabled. Float if not used.		
CLAMP1	E3	5	0	Open-drain FETs which are used for a non-power dissipative overvoltage AC clamp protection.		
CLAMP2 E2 16 O ac		0	When the RECT voltage goes above 15 V, both switches will be turned on and the capacitors will act as a low impedance to protect the device from damage. If used, capacitors are used to connect CLAMP1 to AC1 and CLAMP2 to AC2. Recommended connections are 0.47-µF capacitors.			
COMM1	E4	6	0	Open-drain outputs used to communicate with primary by varying reflected impedance. Connect a		
capacitor from COMM1 to AC1 and a capacitor from COMM2 to AC2 for ca		capacitor from COMM1 to AC1 and a capacitor from COMM2 to AC2 for capacitive load modulation. For resistive modulation connect COMM1 and COMM2 to RECT through a single resistor. See <i>Communication Modulator</i> for more information.				
EN2	G2	11	I	Used to set priority between wireless power and wired power. EN2 low enables wired charging source if AD input voltage is present. EN2 high disables wired charging source and wireless power is enabled if present.		
FOD	F2	14	I	Input for the rectified power measurement. See WPC v1.1 Compatibility for details.		
ILIM	G1	12	I/O	Programming pin for the battery charge current. The total resistance from ILIM to PGND ( $R_{ILIM}$ ) sets the charge current. Figure 32 shows $R_{ILIM}$ to be $R_1 + R_{FOD}$ . Details can be found in <i>Electrical Characteristics</i> and <i>Battery Charge Current Setting Calculations</i> .		
	A1					
	A2	4 00		Device record		
PGND	A3	1, 20	-	Power ground		
	A4					
RECT	C2, C3	18	0	Filter capacitor for the internal synchronous rectifier. Connect a ceramic capacitor to PGND. Depending on the power levels, the value may be from 4.7 $\mu$ F to 22 $\mu$ F.		
TERM	G3	10	I	Input that is used to set the termination threshold. Termination current is the battery current level below which the charge process will cease. The termination current is set as a percentage of the charge current. See <i>Battery Charge Current Setting Calculations</i> for more details.		
TS/CTRL F1 13 I $rs/CTRL$ to ground through a Negative Temperature Coefficient (NTC) resistor. If an N is not desired, connect to PGND with a 10-k $\Omega$ resistor. As a CTRL pin pull low to send transfer (EPT) fault to the transmitter or pull up to an internal rail to send EPT termination.		Temperature Sense (TS) and Control (CTRL) pin functionality. For the TS functionality connect TS/CTRL to ground through a Negative Temperature Coefficient (NTC) resistor. If an NTC function is not desired, connect to PGND with a 10- $k\Omega$ resistor. As a CTRL pin pull low to send end power transfer (EPT) fault to the transmitter or pull up to an internal rail to send EPT termination to the transmitter. See <i>Internal Temperature Sense (TS Function of the TS/CTRL Pin)</i> for more details.				
— — PAD — The exposed thermal pad should be connected to ground (PGND).		PAD	_	The exposed thermal pad should be connected to ground (PGND).		

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# 7 Specifications

# 7.1 Absolute Maximum Ratings<sup>(1)(2)</sup>

over operating free-air temperature range (unless otherwise noted)

		MIN	MAX	UNIT
	RECT, COMM1, COMM2, BAT, CHG, CLAMP1, CLAMP2	-0.3	20	V
	AC1, AC2	-0.8	20	V
Input voltage	AD, AD-EN	-0.3	30	V
	BOOT1, BOOT2	-0.3	26	V
	RECT, COMM1, COMM2, BAT, CHG, CLAMP1, CLAMP2 -0.3   AC1, AC2 -0.8   AD, AD-EN -0.3   BOOT1, BOOT2 -0.3   EN2, TERM, FOD, TS/CTRL, ILIM -0.3   AC1, AC2 BAT   CHG COMM1, COMM2   TJ -40	7	V	
Input current	AC1, AC2		2	A(RMS)
Output current	BAT		1.5	А
Output sink ourrest	CHG		15	mA
	COMM1, COMM2	MM1, COMM2, BAT, CHG, CLAMP1, CLAMP2 -0.3 -0.8 -0.8 -0.3 -0.3 DOT2 -0.3 A, FOD, TS/CTRL, ILIM -0.3	1.0	А
Junction temperature, T	- J	-40	150	°C
Storage temperature, T	tion temperature, T <sub>J</sub>		150	°C

(1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltages are with respect to the VSS terminal, unless otherwise noted.

# 7.2 ESD Ratings

			VALUE	UNIT
V	Electrostatia discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	M
V <sub>(ESD)</sub>	Electrostatic discharge	Charged-device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	±500	v

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

# 7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

				MIN	MAX	UNIT
V <sub>IN</sub>	Input voltage range	RECT	RECT			
I <sub>IN</sub>	Input current	Internal Rectifier (voltage monitore	Internal Rectifier (voltage monitored at RECT node)			
I <sub>BAT</sub>	BAT(output) current	DAT	bq51050B, bq51051B		1.5	^
		BAT	bq51052B		0.8	A
V <sub>AD</sub>	Adapter voltage	AD	AD			
I <sub>AD-EN</sub>	Sink current	AD-EN	AD-EN			
I <sub>COMM</sub>	COMM sink current	СОММ		500	mA	
TJ	Junction temperature			0	125	°C

## 7.4 Thermal Information

		bq51050B, bq5	bq51050B, bq51051B, bq51052B			
	THERMAL METRIC <sup>(1)</sup>	YFP (DSGBA)	RHL (VQFN)	UNIT		
		28 PINS	20 PINS			
$R_{\thetaJA}$	Junction-to-ambient thermal resistance	58.9	37.7	°C/W		
R <sub>0JC(top)</sub>	Junction-to-case (top) thermal resistance	0.2	35.5	°C/W		
$R_{\theta J B}$	Junction-to-board thermal resistance	9.1	13.6	°C/W		
$\Psi_{JT}$	Junction-to-top characterization parameter	1.4	0.5	°C/W		
ΨЈВ	Junction-to-board characterization parameter	8.9	13.5	°C/W		

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report (SPRA953).

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# **Thermal Information (continued)**

		bq51050B, bq510		
	THERMAL METRIC <sup>(1)</sup>	YFP (DSGBA)	RHL (VQFN)	UNIT
		28 PINS	20 PINS	
R <sub>0JC(bot)</sub>	Junction-to-case (bottom) thermal resistance	n/a	2.7	°C/W

## 7.5 Electrical Characteristics

Over junction temperature range  $0^{\circ}C \le T_{J} \le 125^{\circ}C$  and recommended supply voltage (unless otherwise noted)

	PARAMETER	TEST CONDITI	ONS	MIN	TYP	MAX	UNIT
V <sub>UVLO</sub>	Undervoltage lockout	$V_{RECT}: 0 \text{ V} \rightarrow 3 \text{ V}$		2.6	2.7	2.8	V
V <sub>HYS-UVLO</sub>	Hysteresis on UVLO	$V_{RECT}$ : 3 V $\rightarrow$ 2 V			250		mV
V <sub>OVP</sub>	Input overvoltage threshold	$V_{RECT}: 5 \text{ V} \rightarrow 16 \text{ V}$		14.5	15	15.5	V
V <sub>HYS-OVP</sub>	Hysteresis on OVP	$V_{RECT}$ : 16 V $\rightarrow$ 5 V			150		mV
$V_{\text{RECT-REG}}^{(1)}$	V <sub>RECT</sub> regulation voltage				5.11		V
I <sub>LOAD</sub>	$I_{\text{LOAD}}$ Hysteresis for dynamic $V_{\text{RECT}}$ thresholds as a % of $I_{\text{ILIM}}$	I <sub>LOAD</sub> falling			5%		
V <sub>TRACK</sub>	Tracking $V_{\text{RECT}}$ regulation above $V_{\text{BAT}}$	V <sub>BAT</sub> = 3.5 V, I <sub>BAT</sub> ≥ 500 mA			300		mV
V <sub>RECT-REV</sub>	Rectifier reverse voltage protection at the BAT(output)	$V_{RECT-REV} = V_{BAT} - V_{RECT},$ $V_{BAT} = 10 V$			8.3	9	V
V <sub>RECT-DPM</sub>	Rectifier undervoltage protection, restricts $I_{\text{BAT}}$ at $V_{\text{RECT-DPM}}$			3	3.1	3.2	V
QUIESCENT	CURRENT						
	Active chip quiescent current consumption from RECT	$I_{BAT} = 0 \text{ mA}, 0^{\circ}\text{C} \le T_{J} \le 85^{\circ}$	C		8	10	mA
IRECT	(when wireless power is present)	$I_{BAT} = 300 \text{ mA}, 0^{\circ}\text{C} \le T_{J} \le 8$		2	3	mA	
Ι <sub>Q</sub>	Quiescent current at the BAT when wireless power is disabled (Standby)	$V_{BAT} = 4.2 \text{ V}, 0^{\circ}\text{C} \le \text{T}_{\text{J}} \le 85^{\circ}\text{C}$			12	20	μA
ILIM SHORT	PROTECTION						
R <sub>ILIM-SHORT</sub>	Highest value of ILIM resistor considered a fault (short).	$ \begin{array}{c} R_{ILIM} : 200 \ \Omega \rightarrow 50 \ \Omega. \ I_{BAT} \\ latches off, cycle power to \\ reset \end{array} \begin{array}{c} bq51050B, \\ bq51051B \\ bq51052B \end{array} $				120	Ω
	Monitored for $I_{BAT} > I_{LIM\_SHORT, OK}$					235	
t <sub>DGL-Short</sub>	Deglitch time transition from ILIM short to $\mathbf{I}_{\text{BAT}}$ disable				1		ms
I <sub>LIM_SHORT,</sub>	$I_{LIM-SHORT,OK}$ enables the $I_{ILIM}$ short comparator when $I_{BAT}$ is greater than this value	$I_{BAT}$ : 0 mA $\rightarrow$ 200 mA	bq51050B, bq51051B	110	145	165	mA
ОК	BAT is greater than this value	bq51052B		55	75	95	
I <sub>LIM-SHORT,</sub> OK HYSTERESIS	Hysteresis for $I_{\text{LIM-SHORT,OK}}$ comparator	$I_{BAT}$ : 200 mA $\rightarrow$ 0 mA			30		mA
I <sub>BAT-CL</sub>	Maximum output current limit	Maximum I <sub>BAT</sub> that will be d to 1 ms when ILIM is shorte	elivered for up ed to PGND			2.4	А
BATTERY SI	HORT PROTECTION						
V <sub>BAT(SC)</sub>	BAT pin short-circuit detection/precharge threshold	$V_{BAT}:$ 3 V $\rightarrow$ 0.5 V, no degli	itch	0.75	0.8	0.85	V
VBAT(SC)-HYS	V <sub>BAT(SC)</sub> hysteresis	$V_{BAT}$ : 0.5 V $\rightarrow$ 3 V			100		mV
I <sub>BAT(SC)</sub>	Source current to BAT pin during short-circuit	V <sub>BAT</sub> = 0 V	bq51050B, bq51051B	12 18		22	mA
x7	detection		bq51052B	12	18	25	
VOLTAGE R	EGULATION PHASE						
1	I <sub>BAT</sub> threshold during Voltge Regulation Phase that		bq51050B, bq51051B		0.35 * I <sub>BULK</sub>		<b>m</b> A
IEndTrack	changes $V_{\text{RECT}}$ level from $V_{\text{BAT}} + V_{\text{TRACK}}$ to $V_{\text{RECT-REG}}$	I <sub>BAT</sub> decreasing	bq51052B		0.05 * I <sub>BULK</sub>		mA

(1)  $V_{RECT-REG}$  is overridden when rectifier foldback mode is active ( $V_{RECT-REG}$ - $V_{TRACK}$ ).

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STRUMENTS

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# **Electrical Characteristics (continued)**

Over junction temperature range  $0^{\circ}C \le T_{J} \le 125^{\circ}C$  and recommended supply voltage (unless otherwise noted)

	PARAMETER	TEST CONDIT	IONS	MIN	ТҮР	MAX	UNIT
PRECHARG	E						
V <sub>LOWV</sub>	Precharge to fast charge transition threshold	$V_{BAT}\!\!: 2 \; V \to 4 \; V$		2.9	3.0	3.1	
K <sub>PRECHG</sub>	Precharge current as a percentage of the programmed charge current setting $(\mathrm{I}_{\mathrm{BULK}})$	$V_{LOWV} > V_{BAT} > V_{BAT(SC)}$ $I_{BAT}$ : 50 mA - 300 mA	18%	20%	23%	V	
I <sub>PRECHG</sub>	I <sub>BAT</sub> during precharge	$V_{LOWV} > V_{BAT} > V_{BAT(SC)}, I_{I}$	<sub>BULK</sub> = 500 mA		100		mA
t <sub>precharge</sub>	Precharge time-out	$V_{BAT(SC)} < V_{BAT} < V_{LOWV}$			30		min
t <sub>DGL1(LOWV)</sub>	Deglitch time, pre- to fast-charge				25		ms
t <sub>DGL2(LOWV)</sub>	Deglitch time, fast- to precharge				25		ms
OUTPUT							
			bq51050B	4.16	4.20	4.22	
V <sub>OREG</sub>	Regulated BAT(output) voltage	I <sub>BAT</sub> = 1000 mA	bq51051B	4.30	4.35	4.37	V
			bq51052B	4.36	4.40	4.44	
V <sub>DO</sub>	Drop-out voltage, RECT to BAT	I <sub>BAT</sub> = 1 A			110	190	mV
K <sub>ILIM</sub>	Current programming factor	$    R_{LIM} = K_{ILIM} / I_{IBULK} (500 $ mA - 1.5 A)	bq51050B, bq51051B	303	314	321	AΩ
NLIM		$    R_{LIM} = K_{ILIM} / I_{IBULK} (500 $ mA - 1.0 A)	bq51052B	505	514	521	A12
I <sub>BULK</sub>	Battery charging current limits	K <sub>ILIM</sub> 303 to 321	bq51050B, bq51051B	500		1,500	mA
			bq51052B	500		1,000	
t <sub>fast-charge</sub>	Fast-charge timer	$V_{LOWV} < V_{BAT} < V_{BAT-REG}$			10		hours
I <sub>BAT-R</sub>	Battery charge current limit programming range					1500	mA
I <sub>COMM-CL</sub>	Current limit during communication			330	390	420	mA
TERMINATI	ON						
K <sub>TERM</sub>	Programmable termination current as a percentage of $I_{\text{IBULK}}$	R <sub>TERM</sub> = %I <sub>IBULK</sub> x K <sub>TERM</sub> (	200	240	280	Ω/%	
I <sub>TERM-Th</sub>	Termination current from BAT, defined with $K_{\text{TERM}}$ , as the current that terminates the charge cycle	I <sub>BAT</sub> decreasing, R <sub>TERM</sub> = 2 1000 mA		100		mA	
I <sub>TERM</sub>	Constant current at the TERM pin to bias the termination reference		40	50	55	μA	
		bq51050B	V <sub>BAT-REG</sub> –135mV	V <sub>BAT-REG</sub> 110mV	V <sub>BAT-REG</sub> -90mV	V	
V <sub>RECH</sub>	Recharge threshold	bq51051B	V <sub>BAT-REG</sub> –125mV	V <sub>BAT-REG</sub> –95mV	V <sub>BAT-REG</sub> -70mV	v	
		bq51052B	V <sub>BAT-REG</sub> –125mV	V <sub>BAT-REG</sub> –95mV	V <sub>BAT-REG</sub> -70mV		
I <sub>Termination</sub>	Termination current setting limits			120			mA
TS / CTRL P	UNCTIONALITY						
V <sub>TSB</sub>	Internal TS bias voltage ( $V_{TS}$ is the voltage at the TS/CTRL pin, $V_{TSB}$ is the internal bias voltage)	I <sub>TSB</sub> < 100 μA (periodically driven see t <sub>TS/CTRL-Meas</sub> )		2	2.2	2.4	V
V <sub>0C-R</sub>	Rising threshold	$V_{TS}$ : 50% $\rightarrow$ 60%		57	58.7	60	%V <sub>TS</sub>
V <sub>0C-Hyst</sub>	Hysteresis on 0°C Comparator	$V_{TS}$ : 60% $\rightarrow$ 50%			2.4		%V <sub>TSI</sub>
V <sub>10C</sub>	Rising threshold	$V_{TS}$ : 40% $\rightarrow$ 50%		46	47.8	49	%V <sub>TSI</sub>
V <sub>10C-Hyst</sub>	Hysteresis on 10°C Comparator	$V_{TS}$ : 50% $\rightarrow$ 40%			2		%V <sub>TSI</sub>
V <sub>45C</sub>	Falling threshold	$V_{TS}$ : 25% $\rightarrow$ 15%		18	19.6	21	%V <sub>TS</sub>
V <sub>45C-Hyst</sub>	Hysteresis on 45°C Comparator	$V_{\text{TS}}: 15\% \rightarrow 25\%$			3		%V <sub>TS</sub>
V <sub>60C</sub>	Falling threshold	$V_{TS}$ : 20% $\rightarrow$ 5%	12	13.1	14	%V <sub>TSI</sub>	
V <sub>60C-Hyst</sub>	Hysteresis on 60°C Comparator	$V_{TS}$ : 5% $\rightarrow$ 20%			1		%V <sub>TSI</sub>
I <sub>45C</sub>	$I_{\text{BULK}}$ reduction percentage at 45°C (in full JEITA mode - N/A for bq51052B)	$V_{TS}: 25\% \rightarrow 15\%, \ I_{BAT} = I_{E}$	BULK	45%	50%	55%	
		bq51050B			4.06		
V <sub>O-J</sub>	Voltage regulation during JEITA temperature range	bq51051B			4.2		V
		bq51052B			4.2		
V <sub>CTRL-HI</sub>	Voltage on CTRL pin for a high			0.2		5	V

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# **Electrical Characteristics (continued)**

Over junction temperature range $0^{\circ}C \leq T$	≤ 125°C and recommended supply voltage	(unless otherwise noted)

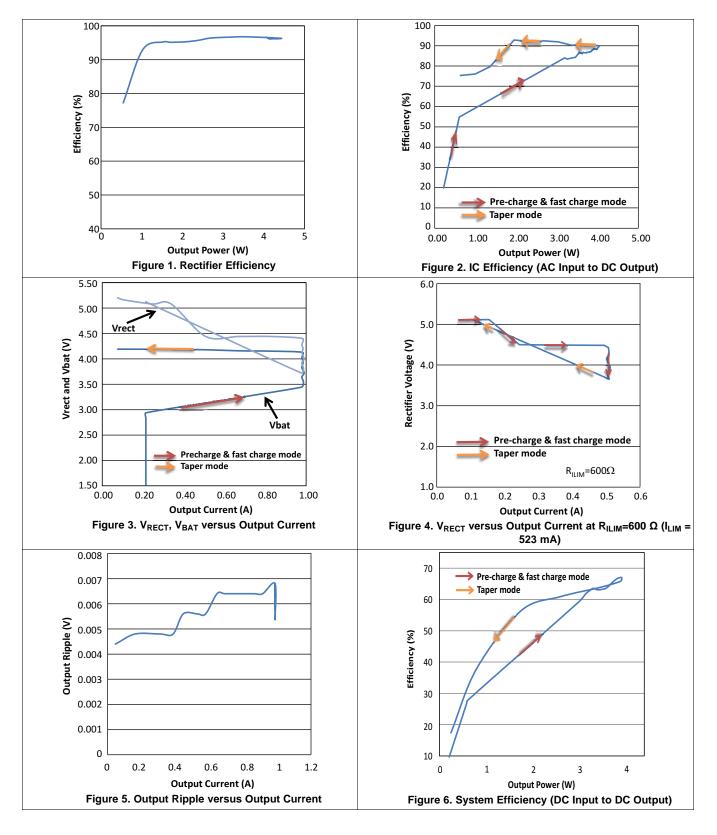
	PARAMETER	TEST CONDITI	ONS	MIN	TYP	MAX	UNIT
V <sub>CTRL-LOW</sub>	Voltage on CTRL pin for a low			0		0.1	V
t <sub>TS/CTRL-Meas</sub>	Time period of TS/CTRL measurements (when $V_{\text{TSB}}$ is being driven internally)	TS bias voltage is only driv communication packets are		24		ms	
t <sub>TS-Deglitch</sub>	Deglitch time for all TS comparators				10		ms
NTC-Pullup	Pullup resistor for the NTC network. Pulled up to the TS bias LDO.			18	20	22	kΩ
NTC-R <sub>NOM</sub>	Nominal resistance requirement at 25°C of the NTC resistor				10		kΩ
NTC-Beta	Beta requirement for accurate temperature sensing through the above specified thresholds				3380		Ω
THERMAL P	ROTECTION	L					
T <sub>J-SD</sub>	Thermal shutdown temperature				155		°C
T <sub>J-Hys</sub>	Thermal shutdown hysteresis				20		°C
OUTPUT LO	GIC LEVELS ON CHG		k				
V <sub>OL</sub>	Open-drain CHG pin	I <sub>SINK</sub> = 5 mA				500	mV
I <sub>OFF,CHG</sub>	CHG leakage current when disabled	V <sub>CHG</sub> = 20 V, 0°C ≤ T <sub>J</sub> ≤ 85°C				1	μA
COMM PIN		-					
R <sub>DS</sub> . ON(COMM)	COMM1 and COMM2	V <sub>RECT</sub> = 2.6 V			1		Ω
f <sub>COMM</sub>	Signaling frequency on COMM pin				2		kb/s
I <sub>OFF,COMM</sub>	COMM pin leakage current	$V_{COMM1} = 20 V,$ $V_{COMM2} = 20 V$			1	μA	
CLAMP PIN			1				
R <sub>DS-</sub> ON(CLAMP)	CLAMP1 and CLAMP2				0.75		Ω
ADAPTER E	NABLE	L					
V <sub>AD-Pres</sub>	V <sub>AD</sub> Rising threshold voltage. EN-UVLO	$V_{AD} \ 0 \ V \rightarrow 5 \ V$		3.5	3.6	3.8	V
V <sub>AD-PresH</sub>	V <sub>AD-Pres</sub> hysteresis, EN-HYS	$V_{AD} 5 V \rightarrow 0 V$			400		mV
I <sub>AD</sub>	Input leakage current	V <sub>RECT</sub> = 0 V, V <sub>AD</sub> = 5 V				60	μA
R <sub>AD</sub>	Pullup resistance from AD-EN to BAT when adapter mode is disabled and VBAT > VAD, EN-OUT	$V_{AD} = 0 \text{ V}, \text{ V}_{BAT} = 5 \text{ V}$			200	350	Ω
V <sub>AD-Diff</sub>	Voltage difference between $V_{\text{AD}}$ and $V_{\text{AD-EN}}$ when adapter mode is enabled, EN-ON	$V_{AD} = 5 \text{ V}, 0^{\circ}\text{C} \le \text{T}_{\text{J}} \le 85^{\circ}\text{C}$		3	4.5	5	V
SYNCHRON	OUS RECTIFIER		I				
I <sub>BAT-SR</sub>	I <sub>BAT</sub> at which the synchronous rectifier enters half	$I_{BAT}$ 200 mA $\rightarrow$ 0 mA	bq51050B, bq51051B	80	115	140	
B/T OK	synchronous mode, SYNC_EN		bq51052B	20	50	65	
I <sub>BAT-SRH</sub>	Hysteresis for I <sub>BAT.SR</sub> (full-synchronous mode enabled)	$I_{BAT}$ 0 mA $\rightarrow$ 200 mA	bq51050B, bq51051B		25		mA
			bq51052B		28		
V <sub>HS-DIODE</sub>	High-side diode drop when the rectifier is in half synchronous mode	$I_{AC-VRECT} = 250 \text{ mA}, \text{ and } T_{J}$	= 25°C		0.7		V
EN2			<b>I</b>				
V <sub>IL</sub>	Input low threshold for EN2					0.4	V
V <sub>IH</sub>	Input high threshold for EN2			1.3			V
R <sub>PD, EN</sub>	EN2 pulldown resistance				200		kΩ
ADC		1					
PowerREC	Received power measurement	0 W – 5 W received power of Rx magnetics losses	after calibration		0.25		W

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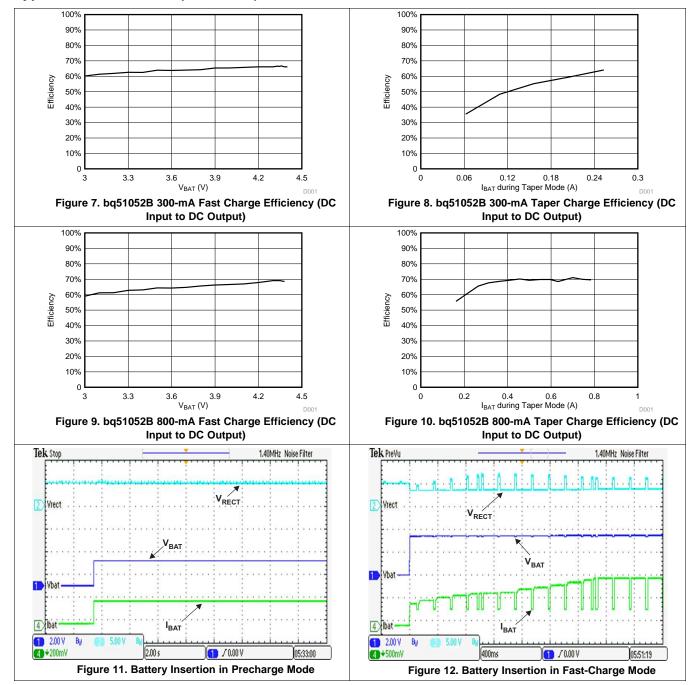
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# 7.6 Typical Characteristics



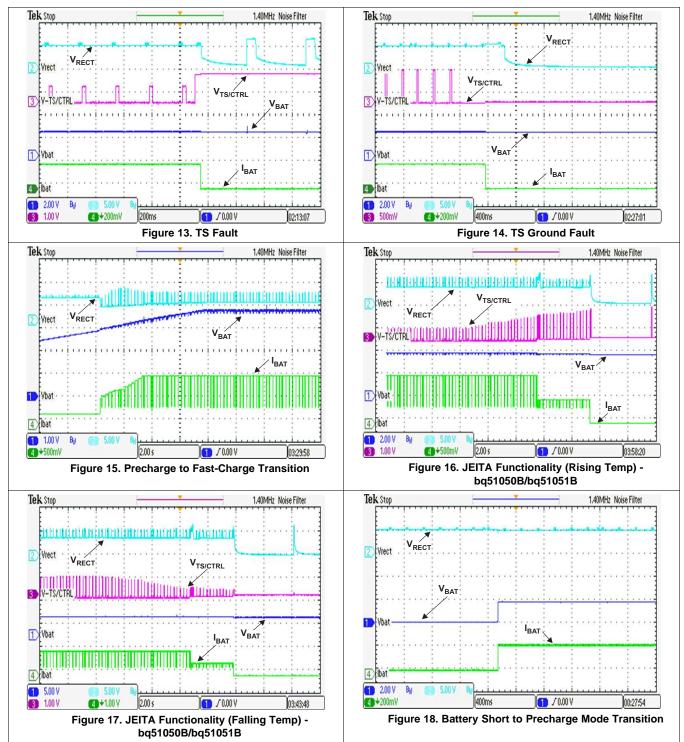


#### **Typical Characteristics (continued)**





## **Typical Characteristics (continued)**





# 8 Detailed Description

## 8.1 Overview

#### 8.1.1 A Brief Description of the Wireless System

A wireless system consists of a charging pad (primary, transmitter) and the secondary-side equipment. There are coils in the charging pad and in the secondary equipment which magnetically couple to each other when the equipment is placed on the charging pad. Power is transferred from the primary to the secondary by transformer action between the coils. Control over the amount of power transferred is achieved by changing the frequency of the primary drive.

The secondary can communicate with the primary by changing the load seen by the primary. This load variation results in a change in the primary coil current, which is measured and interpreted by a processor in the charging pad. The communication is digital - packets are transferred from the secondary to the primary. Differential biphase encoding is used for the packets. The rate is 2-kbps.

Various types of communication packets have been defined. These include identification and authentication packets, error packets, control packets, power usage packets, end of power packet and efficiency packets.

The primary coil is powered off most of the time. It wakes up occasionally to see if a secondary is present. If a secondary authenticates itself to the primary, the primary remains powered up. The secondary maintains full control over the power transfer using communication packets.

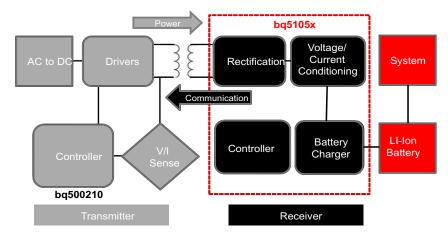


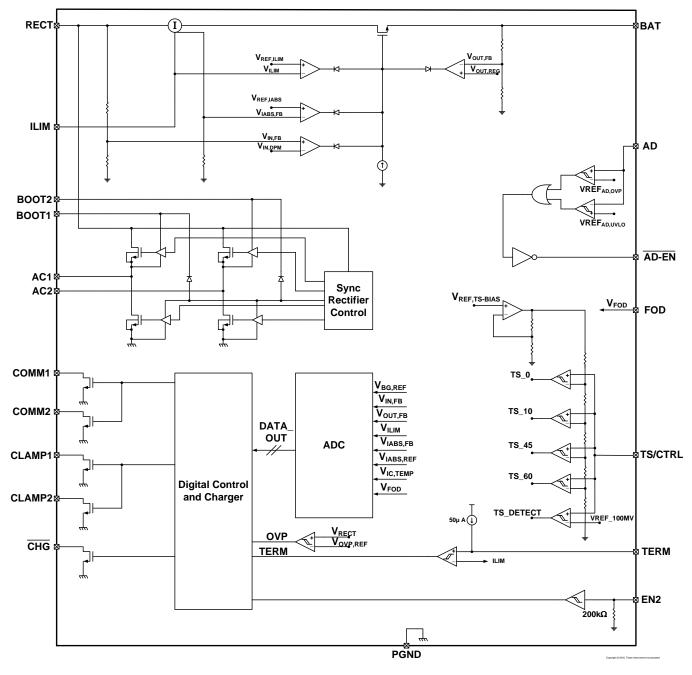
Figure 19. WPC Wireless Power Charging System Indicating the Functional Integration of the bq5105x

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# 8.2 Functional Block Diagram



# 8.3 Feature Description

#### 8.3.1 Using the bq5105x as a Wireless Li-Ion/Li-Pol Battery Charger (With Reference to Functional Block Diagram)

Functional Block Diagram is the schematic of a system which uses the bq5105x as a direct battery charger. When the system shown in Functional Block Diagram is placed on the charging pad (transmitter), the receiver coil couples to the magnetic flux generated by the coil in the charging pad which consequently induces a voltage in the receiver coil. The internal synchronous rectifier feeds this voltage to the RECT pin which has the filter capacitor  $C_3$ .

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#### **Feature Description (continued)**

The bq5105x identifies and authenticates itself to the primary using the COMM pins by switching on and off the COMM FETs and hence switching in and out  $C_{COMM}$ . If the authentication is successful, the transmitter will remain powered on. The bq5105x measures the voltage at the RECT pin, calculates the difference between the actual voltage and the desired voltage  $V_{RECT-REG}$  and sends back error packets to the primary. This process goes on until the RECT voltage settles at  $V_{RECT-REG}$ .

During power-up, the LDO is held off until the  $V_{RECT-REG}$  threshold converges. The voltage control loop ensures that the output (BAT) voltage is maintained at  $V_{BAT-REG}$ . The values of  $V_{BAT}$  and  $V_{RECT}$  are dependant on the battery charge mode. The bq5105x continues to monitor the  $V_{RECT}$  and  $V_{BAT}$  and sends error packets to the primary every 250 ms. The bq5105x regulates the  $V_{RECT}$  voltage very close to battery voltage, this voltage tracking process minimizes the voltage difference across the internal LDO and maximizes the charging efficiency. If a large transient occurs, the feedback to the primary speeds up to every 32 ms in order to converge on an operating point in less time.

#### 8.3.2 Details of a Qi Wireless Power System and bq5105xB Power Transfer Flow Diagrams

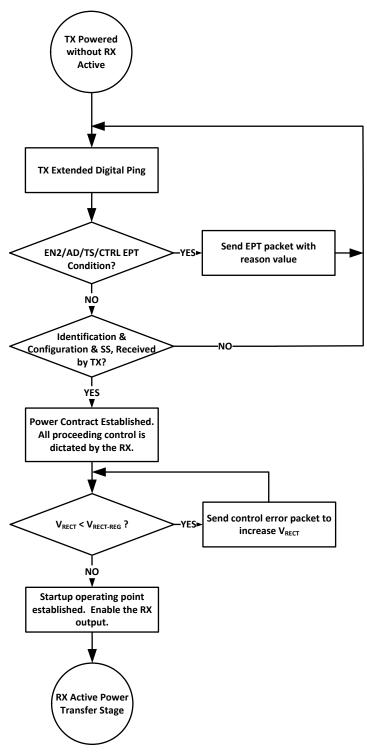
The bq5105xB integrates a fully compliant WPC v1.1 communication algorithm in order to streamline receiver designs (no extra software development required). Other unique algorithms such as Dynamic Rectifier Control are also integrated to provide best-in-class system performance. This section provides a high level overview of these features by illustrating the wireless power transfer flow diagram from start-up to active operation.

During start-up operation, the wireless power receiver must comply with proper handshaking to be granted a power contract from the TX. The TX will initiate the handshake by providing an extended digital ping. If an RX is present on the TX surface, the RX will then provide the signal strength, configuration and identification packets to the TX (see volume 1 of the WPC specification for details on each packet). These are the first three packets sent to the TX. The only exception is if there is a shutdown condition on the EN1/EN2, AD, or TS/CTRL pins where the Rx will shut down the TX immediately. Once the TX has successfully received the signal strength, configuration and identification packets, the RX will be granted a power contract and is then allowed to control the operating point of the power transfer. With the use of the bq5105xB Dynamic Rectifier Control algorithm, the RX will inform the TX to adjust the rectifier voltage above 5 V before enabling the output supply. This method enhances the transient performance during system start-up. See Figure 20 for the start-up flow diagram details.

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### Feature Description (continued)





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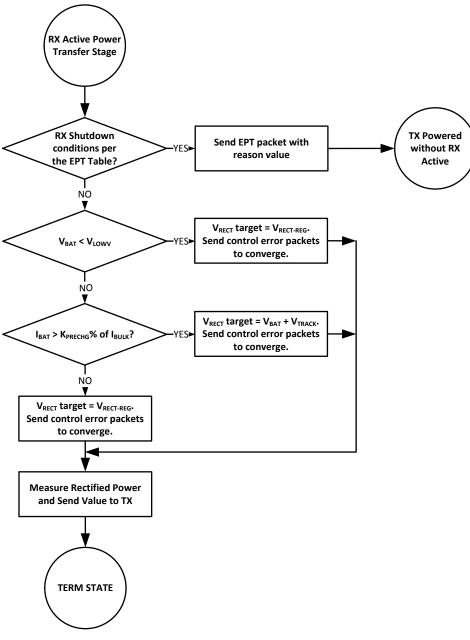


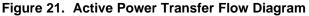
#### **bq51050B**, **bq51051B**, **bq51052B** SLUSB42E – JULY 2012 – REVISED MARCH 2015

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#### Feature Description (continued)

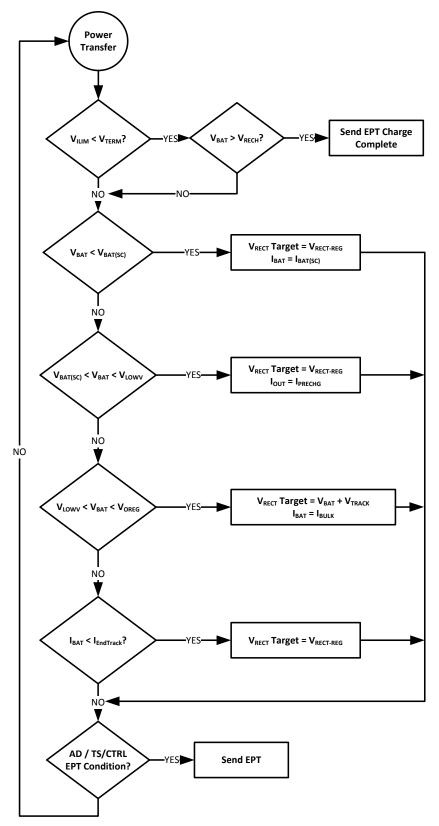
Once the start-up procedure has been established, the RX will enter the active power transfer stage. This is considered the "main loop" of operation. The Dynamic Rectifier Control algorithm will determine the rectifier voltage target based on a percentage of the maximum output current level setting (set by  $K_{ILIM}$  and the  $I_{ILIM}$  resistance to PGND). The RX will send control error packets in order to converge on these targets. As the output current changes, the rectifier voltage target will dynamically change. As a note, the feedback loop of the WPC system is relatively slow where it can take up to 90 ms to converge on a new rectifier voltage target. It should be understood that the instantaneous transient response of the system is open loop and dependent on the RX coil output impedance at that operating point. More details on this will be covered in the section Receiver Coil Load-Line Analysis. The "main loop" will also determine if any conditions are true and will then discontinue the power transfer. Figure 21 shows the active power transfer loop.







# Feature Description (continued)







#### Feature Description (continued)

#### 8.3.3 Battery Charge Profile

The battery is charged in three phases: precharge, fast-charge constant current and constant voltage. A voltagebased battery pack thermistor monitoring input (TS function of the TS/CTRL pin) is included that monitors battery temperature for safe charging. The TS function for bq51050B and bq51051B is JEITA compatible. The TS function for the bq51052B modifies the current regulation differently than standard JEITA. See *Battery-Charger Safety and JEITA Guidelines* for more details.

The rectifier voltage follows BAT voltage plus  $V_{TRACK}$  for any battery voltage above  $V_{LOWV}$  to full regulation voltage and most of the taper charging phase. If the battery voltage is below  $V_{LOWV}$  the rectifier voltage increases to  $V_{RECT-REG}$ .

If I<sub>BAT</sub> is less than I<sub>EndTrack</sub> (a percentage of I<sub>BULK</sub>) during taper mode, the rectifier voltage increases to V<sub>RECT-REG</sub>.

The charge profile for the bq51050B and bq51051B is shown in Figure 23 while the bq51052B is shown in Figure 24.

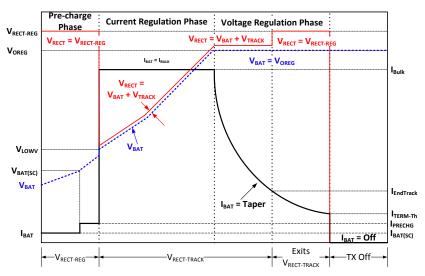


Figure 23. bq51050B and bq51051B Li-Ion Battery Charge Profile

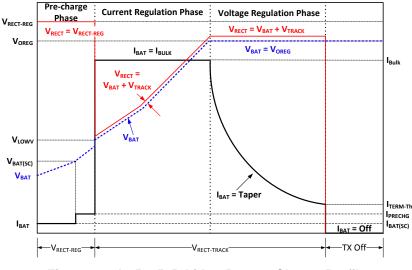


Figure 24. bq51052B Li-Ion Battery Charge Profile

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#### Feature Description (continued)

#### 8.3.4 Battery Charging Process

#### 8.3.4.1 Precharge Mode ( $V_{BAT} \leq V_{LOWV}$ )

The bq5105X enters precharge mode when  $V_{BAT} \le V_{LOWV}$ . Upon entering precharge mode, battery charge current limit is set to  $I_{PRECHG}$ . During precharge mode, the charge current is regulated to  $K_{PRECHG}$  percent of the fast charge current ( $I_{BULK}$ ) setting. For example, if IBULK is set to 800 mA, then the precharge current would have a typical value of 160 mA.

If the battery is deeply discharged or shorted ( $V_{BAT} < V_{BAT(SC)}$ ), the bq5105X applies  $I_{BAT(SC)}$  current to bring the battery voltage up to acceptable charging levels. Once the battery rises above  $V_{BAT(SC)}$ , the charge current is regulated to  $I_{PRECHG}$ .

Under normal conditions, the time spent in this precharge region is a very short percentage of the total charging time and this does not affect the overall charging efficiency for very long.

#### 8.3.4.2 Fast Charge Mode / Constant Voltage Mode

Once  $V_{BAT} > V_{LOWV}$ , the bq5105x enters fast charge mode (Current Regulation Phase) where charge current is regulated using the internal MOSFETs between RECT and BAT. Once the battery voltage charges up to  $V_{BAT}$ -REG, the bq5105x enters constant voltage (CV) phase and regulates battery voltage to  $V_{OREG}$  and the charging current is reduced.

Once  $I_{BAT}$  falls below the termination threshold ( $I_{TERM-Th}$ ), the charger sends an EPT (Charge Complete) notification to the TX and enters high impedance mode.

#### 8.3.4.3 Battery Charge Current Setting Calculations

#### 8.3.4.3.1 R<sub>ILIM</sub> Calculations

The bq5105x includes a means of providing hardware overcurrent protection by means of an analog current regulation loop. The hardware current limit provides an extra level of safety by clamping the maximum allowable output current (for example, a current compliance). The calculation for the total R<sub>ILIM</sub> resistance is as follows:

$$R_{1} = \frac{K_{ILIM}}{I_{BULK}} - R_{FOD} \qquad \qquad R_{ILIM} = R_{1} + R_{FOD} \qquad \qquad I_{BULK} = \frac{K_{ILIM}}{R_{ILIM}}$$
(1)

Where  $I_{BULK}$  is the programmed battery charge current during fast charge mode. When referring to the application diagram shown in Figure 32,  $R_{ILIM}$  is the sum of  $R_{FOD}$  and  $R_1$  (the total resistance from the ILIM pin to PGND).

#### 8.3.4.3.2 Termination Calculations

The bq5105X includes a programmable upper termination threshold. The upper termination threshold is calculated using Equation 2:

$$R_{\text{TERM}} = K_{\text{TERM}} * \% I_{\text{BULK}}$$

$$\%I_{BULK} = \frac{R_{TERM}}{K_{TERM}}$$
(2)

The  $K_{\text{TERM}}$  constant is specified in *Electrical Characteristics* as 240  $\Omega$ /%. The upper termination threshold is set as a percentage of the charge current setting ( $I_{\text{BULK}}$ ).

For example, if  $R_{ILIM}$  is set to 314  $\Omega$ ,  $I_{BULK}$  will be 1 A (314 ÷ 314). If the upper termination threshold is desired to be 100 mA, this would be 10% of  $I_{BULK}$ . The  $R_{TERM}$  resistor would then equal 2.4 k $\Omega$  (240 × 10).

Termination can be disabled by floating the TERM pin. If the TERM pin is grounded the termination function is effectively disabled. However, due to offsets of internal comparators, termination may occur at low battery currents.



#### Feature Description (continued)

#### 8.3.4.4 Battery-Charger Safety and JEITA Guidelines

The bq5105x continuously monitors battery temperature by measuring the voltage between the TS/CTRL pin and PGND. A negative temperature coefficient thermistor (NTC) and an external voltage divider typically develop this voltage. The bq5105x compares this voltage against its internal thresholds to determine if charging is allowed. To initiate a charge cycle, the voltage on TS/CTRL pin ( $V_{TS}$ ) must be within the  $V_{T1}$  to  $V_{T4}$  thresholds. If  $V_{TS}$  is outside of this range, the bq5105x suspends charge and waits until the battery temperature is within the  $V_{T1}$  to  $V_{T4}$  range. Additional information on the Temperature Sense function can be found in *Internal Temperature Sense (TS Function of the TS/CTRL Pin)*.

#### 8.3.4.4.1 bq51050B and bq51051B JEITA

If  $V_{TS}$  is within the ranges of  $V_{T1}$  and  $V_{T2}$  or  $V_{T3}$  and  $V_{T4}$ , the charge current is reduced to  $I_{BULK}/2$ . If  $V_{TS}$  is within the range of  $V_{T1}$  and  $V_{T3}$ , the maximum charge voltage regulation is  $V_{OREG}$ . If  $V_{TS}$  is within the range of  $V_{T3}$  and  $V_{T4}$ , the maximum charge voltage regulation is reduced to "NEW SPEC". Figure 25 summarizes the operation.

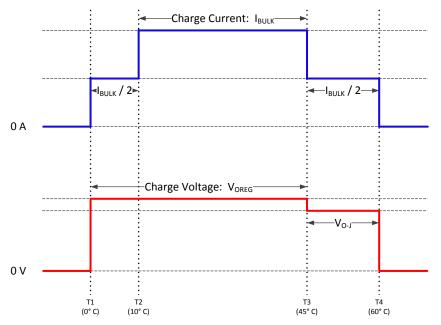


Figure 25. JEITA Compatible TS Profile for bq51050B and bq51051B

#### 8.3.4.4.2 bq51052B Modified JEITA

The bq51052B has a modified JEITA profile. The maximum charge current is not modified between  $V_{T1}$  and  $V_{T2}$  or between  $V_{T3}$  and  $V_{T4}$ , it remains at  $I_{BULK}$ . The maximum charge voltage is reduced to  $V_{O-J}$  when the  $V_{TS}$  is between  $V_{T3}$  and  $V_{T4}$ .

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## Feature Description (continued)

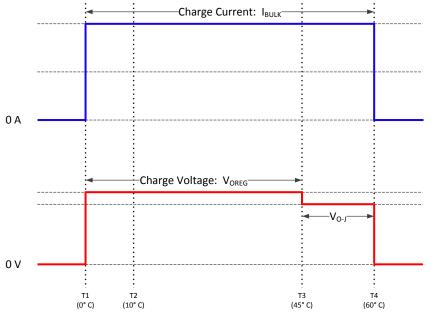


Figure 26. JEITA Compatible TS Profile for bq51052B

#### 8.3.4.5 Input Overvoltage

If, for some condition (for example, a change in position of the equipment on the charging pad), the rectifier voltage suddenly increases in potential, the voltage-control loop inside the bq5105x becomes active, and prevents the output from going beyond  $V_{BAT-REG}$ . The receiver then starts sending back error packets every 32 ms until the RECT voltage comes back to an acceptable level, and then maintains the error communication every 250 ms.

If the input voltage increases in potential beyond  $V_{OVP}$ , the device switches off the internal FET and communicates to the primary to bring the voltage back to  $V_{RECT-REG}$ . In addition a proprietary voltage protection circuit is activated by means of  $C_{CLAMP1}$  and  $C_{CLAMP2}$  that protects the device from voltages beyond the maximum rating.

#### 8.3.4.6 End Power Transfer Packet (WPC Header 0x02)

The WPC allows for a special command to terminate power transfer from the TX termed End Power Transfer (EPT) packet. WPC v1.1 specifies the reasons for sending a termination packet and their data field value. In Table 1, the CONDITION column corresponds to the stimulus causing the bq5105x device to send the hexidecimal code in the VALUE column.

REASON	VALUE	CONDITION
Unknown	0x00	$AD > V_{AD-Pres}$ , TS/CTRL = $V_{CTRL-HI}$
Charge Complete	0x01	IBAT falls below ITERM-Th during Taper mode
Internal Fault	0x02	$T_J > 150^{\circ}C$ or $R_{ILIM} < R_{ILIM-SHORT}$
Overtemperature	0x03	TS < $V_{HOT}$ , TS > $V_{COLD}$ , or TS/CTRL < $V_{CTRL-LOW}$
Overvoltage	0x04	Not Sent
Overcurrent	0x05	Not Sent
Battery failure	0x06	Battery is not coming out of precharge mode after Precharge time-out, or fast charge time-out has occured.
Reconfigure	0x07	Not Sent
No Response	0x08	V <sub>RECT</sub> target does not converge



#### 8.3.4.7 Status Output

The bq5105x provides one status output,  $\overline{CHG}$ . This output is an open-drain NMOS device that is rated to 20 V. The open-drain FET connected to the CHG pin will be turned on whenever the output (BAT) of the charger is enabled. As a note, the output of the charger supply will not be enabled if the V<sub>RECT-REG</sub> does not converge to the no-load target voltage.

#### 8.3.4.8 Communication Modulator

The bq5105x provides two identical, integrated communication FETs which are connected to the pins COMM1 and COMM2. These FETs are used for modulating the secondary load current which allows bq5105x to communicate error control and configuration information to the transmitter. There are two methods to implement load modulation, capacitive and resistive.

Capacitive load modulation is more commonly used. Capacitive load modulation is shown in Figure 27. In this case, a capacitor is connected from COMM1 to AC1 and from COMM2 to AC2. When the COMM switches are closed there is effectively a 22 nF capacitor connected between AC1 and AC2. Connecting a capacitor in between AC1 and AC2 modulates the impedance seen by the coil, which will be reflected to the primary and interpreted by the controller as a change in current.

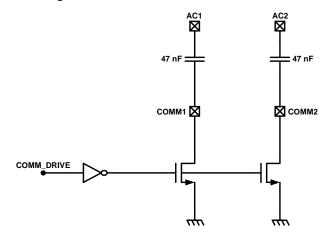


Figure 27. Capacitive Load Modulation

Figure 28 shows how the COMM pins can be used for resistive load modulation. Each COMM pin can handle at most a 24  $\Omega$  communication resistor. Therefore, if a COMM resistor between 12  $\Omega$  and 24  $\Omega$  is required, COMM1 and COMM2 pins must be connected in parallel. bq5105x does not support a COMM resistor less than 12  $\Omega$ .

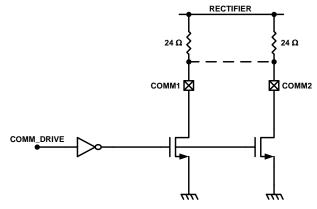


Figure 28. Resistive Load Modulation

### bq51050B, bq51051B, bq51052B

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#### 8.3.4.9 Synchronous Rectification

The bq5105x provides an integrated, self-driven synchronous rectifier that enables high-efficiency AC to DC power conversion. The rectifier consists of an all NMOS H-Bridge driver where the back gates of the diodes are configured to be the rectifier when the synchronous rectifier is disabled. During the initial start-up of the WPC system the synchronous rectifier is not enabled. At this operating point, the DC rectifier voltage is provided by the diode rectifier. Once  $V_{RECT}$  is greater than  $V_{UVLO}$ , half synchronous mode will be enabled until the load current surpasses  $I_{BAT-SR}$ . Above  $I_{BAT-SR}$  the full synchronous rectifier stays enabled until the load current drops back below the hysteresis level ( $I_{BAT-SRH}$ ) where half synchronous mode is re-enabled.

### 8.3.4.10 Internal Temperature Sense (TS Function of the TS/CTRL Pin)

The bq5105x includes a ratiometric battery temperature sense circuit. The temperature sense circuit has two ratiometric thresholds which represent hot and cold conditions. An external temperature sensor is recommended to provide safe operating conditions to the receiver product. This pin is best used when monitoring the battery temperature.

The circuits in Figure 29 allow for any NTC resistor to be used with the given  $V_{HOT}$  and  $V_{COLD}$  thresholds. The thermister characteristics and threshold temperatures selected will determine which circuit is best for an application.

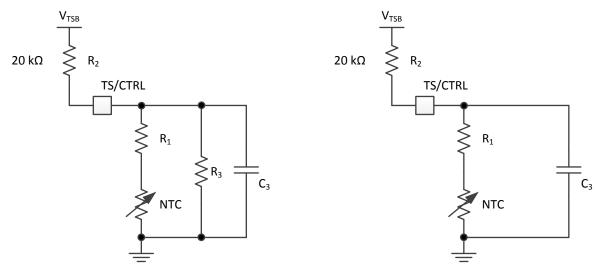


Figure 29. NTC Circuit Options for Safe Operation of the Wireless Receiver Power Supply

The resistors R1 and R3 can be solved by resolving the system of equations at the desired temperature thresholds. The two equations are:

$$%V_{COLD} = \frac{\left(\frac{R_{3}\left(R_{NTC}|_{TCOLD} + R_{1}\right)}{R_{3} + \left(R_{NTC}|_{TCOLD} + R_{1}\right)}\right)}{\left(\frac{R_{3}\left(R_{NTC}|_{TCOLD} + R_{1}\right)}{R_{3} + \left(R_{NTC}|_{TCOLD} + R_{1}\right)}\right) + R2} \times 100$$
  
%V\_{HOT} = 
$$\frac{\left(\frac{R_{3}\left(R_{NTC}|_{THOT} + R_{1}\right)}{R_{3} + \left(R_{NTC}|_{THOT} + R_{1}\right)}\right)}{\left(\frac{R_{3}\left(R_{NTC}|_{THOT} + R_{1}\right)}{R_{3} + \left(R_{NTC}|_{THOT} + R_{1}\right)}\right) + R2} \times 100$$

(3)







Where:

$$R_{\text{NTC}}|_{\text{TCOLD}} = R_{o}e^{\beta \left(\frac{1}{1} + COLD} - \frac{1}{1} + T_{o}\right)}$$
$$R_{\text{NTC}}|_{\text{THOT}} = R_{o}e^{\beta \left(\frac{1}{1} + HOT} - \frac{1}{1} + T_{o}\right)}$$

 $T_{COLD}$  and  $T_{HOT}$  are the desired temperature thresholds in degrees Kelvin.  $R_o$  is the nominal resistance at  $T_0$  (25°C) and  $\beta$  is the temperature coefficient of the NTC resistor. An example solution for part number ERT-JZEG103JA is:

R<sub>1</sub> = 29.402 kΩ R<sub>3</sub> = 14.302 kΩ

Where,

 $T_{COLD} = 0^{\circ}C (273.15^{\circ}K)$  $T_{HOT} = 60^{\circ}C (333.15^{\circ}K)$  $\beta = 3380$  $R_{o} = 10 k\Omega$ 

The plot of the percent  $V_{TSB}$  versus temperature is shown in Figure 30:

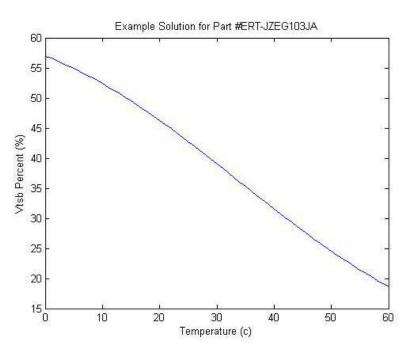


Figure 30. Example Solution for Panasonic Part # ERT-JZEG103JA

Figure 31 shows the periodic biasing scheme used for measuring the TS state. An internal TS\_READ signal enables the TS bias voltage for 25 ms. During this period the TS comparators are read (each comparator has a 10-ms deglitch) and appropriate action is taken based on the temperature measurement. After this 25-ms period has elapsed the TS\_READ signal goes low, which causes the TS/CTRL pin to become high impedance. During the next 100-ms period, the TS voltage is monitored and compared to  $V_{CTRL-HI}$ . If the TS voltage is greater than  $V_{CTRL-HI}$  then a secondary device is driving the TS/CTRL pin and a CTRL = 1 is detected.



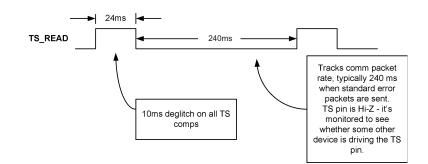


Figure 31. Timing Diagram for TS Detection Circuit

#### 8.3.4.10.1 TS/CTRL Function

The TS/CTRL pin offers three functions:

- NTC temperature monitoring
- Charge done indication
- Fault indication

When an NTC resistor is connected between the TS/CTRL pin and PGND, the NTC function is allowed to operate. This functionality can effectively be disabled by connecting a 10 k $\Omega$  resistor from TS/CRTL to PGND. If the TS/CTRL pin is pulled above  $V_{CTRL-HI}$ , the RX is shut down with the indication of a charge complete condition. If the TS/CTRL pin is pulled below  $V_{CTRL-LOW}$ , the RX is shut down with the indication of a fault.

8.3.4.10.2 Thermal Protection

The bq5105x includes thermal shutdown protection. If the die temperature reaches  $T_{J-SD}$ , the LDO is shut off to prevent any further power dissipation. Once the temperature falls  $T_{J-Hvs}$  below  $T_{J-SD}$ , operation can continue.

#### 8.3.4.11 WPC v1.1 Compatibility

The bq5105x is a WPC v1.1 compatible device. In order to enable a Power Transmitter to monitor the power loss across the interface as one of the possible methods to limit the temperature rise of Foreign Objects, the bq5105x reports its Received Power to the Power Transmitter. The Received Power equals the power that is available from the output of the Power Receiver plus any power that is lost in producing that output power. For example, the power loss includes (but is not limited to) the power loss in the Secondary Coil and series resonant capacitor, the power loss in the Shielding of the Power Receiver, the power loss in the rectifier, the power loss in any post-regulation stage, and the eddy current loss in metal components or contacts within the Power Receiver. In the WPC v1.1 specification, foreign object detection (FOD) is enforced, that means the bq5105x will send received power information with known accuracy to the transmitter.

WPC v1.1 defines Received Power as "the average amount of power that the Power Receiver receives through its Interface Surface, in the time window indicated in the Configuration Packet".

A Receiver will be certified as WPC v1.1 only after meeting the following requirement. The device under test (DUT) is tested on a Reference Transmitter whose transmitted power is calibrated, the receiver must send a received power such that:

0 < (TX PWR) REF – (RX PWR out) DUT < 375 mW

(5)

This 250 mW bias ensures that system will remain interoperable.

WPC v1.1 Transmitters will be tested to see if they can detect reference Foreign Objects with a Reference receiver. The WPC v1.1 specification allows much more accurate sensing of Foreign Objects than WPC v1.0.

A Transmitter can be certified as a WPC v1.1 only after meeting the following requirement. A Transmitter is tested to see if it can prevent some reference Foreign Objects (disc, coin, foil) from exceeding their threshold temperature (60°C, 80°C).



#### 8.4 Device Functional Modes

The general modes of battery charging are described above in the *Feature Description*. The bq5105x devices have several functional modes. Start-up refers to the initial power transfer and communication between the receiver (bq5105x circuit) and the transmitter. Power transfer refers to any time that the TX and RX are communicating and power is being delivered from the TX to the RX. Charge termination covers intentional termination (charge complete) and unintentional termination (removal of the RX from the TX, over temperature or other fault conditions).

Texas

**NSTRUMENTS** 

# 9 Application and Implementation

#### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

## 9.1 Application Information

The bq51050B is an integrated wireless power receiver and charger in a single device. The device complies with the WPC v1.1 specifications for a wireless power receiver. When paired with a WPC v1.1 compliant transmitter, it can provide up to 5-W of power for battery charging. There are several tools available for the design of the system. These tools may be obtained by checking the product page at www.ti.com/product/bq51050b.

# 9.2 Typical Application

## 9.2.1 bq51050B Used as a Wireless Power Receiver and Li-Ion/Li-Pol Battery Charger

The following application discussion covers the requirements for setting up the bq51050B in a Qi-compliant system for charging a battery.

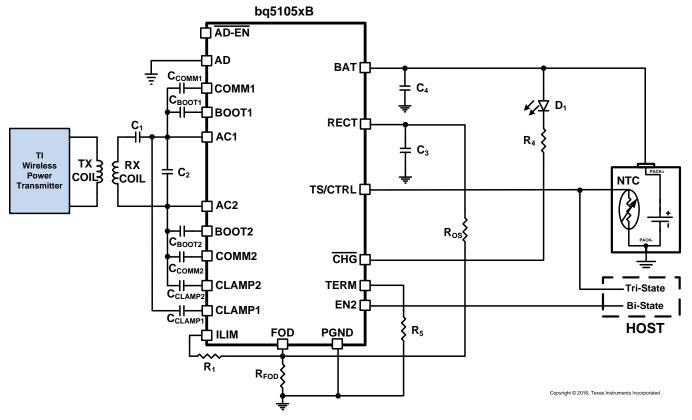


Figure 32. Typical Application Schematic

# 9.2.1.1 Design Requirements

This application is for a 4.2-V Lithium-Ion battery to be charged at 800 mA. Because this is planned for a WPC v1.1 solution, any of the Qi-certified transmitters can be used interchangeably so no discussion of the TX is required. To charge a 4.20-V Li-Ion battery, the bq51050B will be chosen. Each of the components from the application drawing will be examined. Temperature sensing of the battery must be done with JEITA specifications. An LED indicator is required to notify the user if charging is active.



## Typical Application (continued)

#### 9.2.1.2 Detailed Design Procedure

#### 9.2.1.2.1 Series and Parallel Resonant Capacitor Selection

Shown in Figure 33, the capacitors C1 (series) and C2 (parallel) make up the dual resonant circuit with the receiver coil. These two capacitors must be sized correctly per the WPC v1.1 specification. Figure 33 shows the equivalent circuit of the dual resonant circuit:

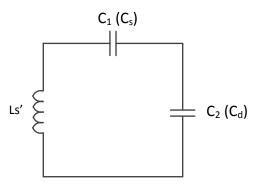
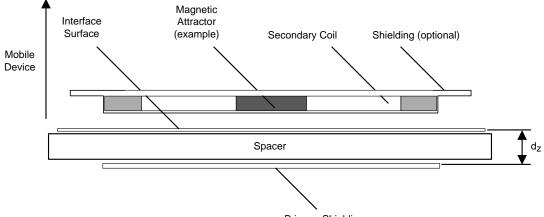


Figure 33. Dual Resonant Circuit with the Receiver Coil

The power receiver design requirements in volume 1 of the WPC v1.1 specification highlights in detail the sizing requirements. To summarize, the receiver designer will be required take inductance measurements with a fixed test fixture. The test fixture is shown in Figure 34:



Primary Shielding

Figure 34. WPC v1.1 Receiver Coil Test Fixture for the Inductance Measurement Ls'

The primary shield is to be 50 mm  $\times$  50 mm  $\times$  1 mm of Ferrite material PC44 from TDK Corp. The gap (dZ) is to be 3.4 mm. The receiver coil, as it will be placed in the final system (for example, the back cover and battery must be included if the system calls for this), is to be placed on top of this surface and the inductance is to be measured at 1-V RMS and a frequency of 100 kHz. This measurement is termed Ls'. The measurement termed Ls is the free-space inductance. Each capacitor can then be calculated using Equation 6:

$$C_{1} = \frac{1}{(2\pi \times fs)^{2} \times L'_{s}}$$
$$C_{2} = \left( (f_{D} \times 2\pi)^{2} \times L_{s} - \frac{1}{C_{1}} \right)^{-1}$$

Where  $f_S$  is 100 kHz +5/–10% and  $f_D$  is 1 MHz ±10%. C<sub>1</sub> must be chosen first prior to calculating C<sub>2</sub>. The quality factor must be greater than 77 and can be determined by Equation 7:

(6)

**bq51050B**, **bq51051B**, **bq51052B** SLUSB42E – JULY 2012–REVISED MARCH 2015

## **Typical Application (continued)**

$$\mathsf{Q} = \frac{2\pi \times f_{\mathsf{D}} \times \mathsf{Ls}}{\mathsf{R}}$$

Where R is the DC resistance of the receiver coil. All other constants are defined above.

For this application, we will design with an inductance measurement (L) of 11  $\mu$ H and an Ls' of 16  $\mu$ H with a DC resistance of 191 mΩ. Plugging Ls' into Equation 6 above, we get a value for C<sub>1</sub> to be 158.3 nF. The range on the capacitance is about 144 nF to 175 nF. To build the resulting value, the optimum solution is usually found with 3 capacitors in parallel. This allows for more precise selection of values, lower effective resistance and better thermal results. To get 158 nF, choose from standard values. In this case, the values are 68 nF, 47 nF and 39 nF for a total of 154 nF. Well in the required range. Now that C<sub>1</sub> is chosen, the value of C<sub>2</sub> can be calculated. The result of this calculation is 2.3 nF. The practical solution for this is 2 capacitors, a 2.2 nF capacitor and a 100 pF capacitor. In all cases, these capacitors must have at least a 25-V rating. Solving for the quality factor (Q) this solution shows a rating over 500.

#### 9.2.1.2.2 COMM, CLAMP and BOOT Capacitors

For most applications, the COMM, CLAMP and BOOT capacitors will be chosen to match the Evaluation Module.

The BOOT capacitors are used to allow the internal rectifier FETs to turn on and off properly. These capacitors are on the AC1 or AC2 lines to the Boot nodes and should have a minimum of 10-V rating. A 10-nF capacitor with a 10-V rating is chosen.

The CLAMP capacitors are used to aid the clamping process to protect against overvoltage. Choosing a 0.47-µF capacitor with a 25-V rating is appropriate for most applications.

The COMM capacitors are used to facilitate the communication from the RX to the TX. This selection can vary a bit more than the BOOT and CLAMP capacitors. In general, a 22-nF capacitor is recommended. Based on the results of testing of the communication robustness, a change to a 47-nF capacitor may be in order. The larger the capacitor the larger the deviation will be on the coil which sends a stronger signal to the TX. This also decreases the efficiency somewhat. In this case, choose the 22-nF capacitor with the 25-V rating.

#### 9.2.1.2.3 Charging and Termination Current

The Design Requirements show an 800-mA charging current and an 80-mA termination current.

Setting the charge current ( $I_{BULK}$ ) is done by selecting the  $R_1$  and  $R_{FOD}$ . Solving Equation 1 results in  $R_{ILIM}$  of 393  $\Omega$ . Setting  $R_{FOD}$  to 200  $\Omega$  as a starting point before the FOD calibration is recommended. This leaves 205  $\Omega$  for  $R_1$ . Using standard resistor values (or resistors in series / parallel) can improve accuracy.

Setting the termination current is done with Equation 2. Because 80 mA is 10% of the  $I_{BULK}$  (800mA), the  $R_{TERM}$  is calculated as (240 \* 10) or 2.4 k $\Omega$ .

#### 9.2.1.2.4 Adapter Enable

<u>The AD</u> pin will be tied to the external USB power source to allow for an external source to power the system. AD\_EN is tied to the gate of Q1 (CSD75205W1015). This allows the bq51050B to sense when power is applied to the AD pin. The EN2 pin controls whether the wired source will be enabled or not. EN2 is tied to the system host to allow it to control the use of the USB power. If wired power is enabled and present, the AD pin will disable the BAT output and then enable Q1 through the AD\_EN pin. An external charger is required to take control of the battery charging.

#### 9.2.1.2.5 Charge Indication and Power Capacitors

The  $\overline{CHG}$  pin is open-drain. D<sub>1</sub> and R<sub>4</sub> are selected as a 2.1-V forward bias capable of 2 mA and a 100- $\Omega$  current-limiting resistor.

RECT is used to smooth the internal AC to DC conversion. Two 10- $\mu$ F capacitors and a 0.1- $\mu$ F capacitor are chosen. The rating is 25 V.

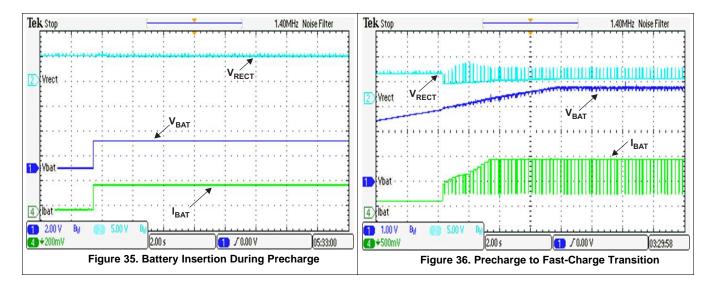
BAT capacitors are 1.0  $\mu$ F and 0.1  $\mu$ F.

(7)



# **Typical Application (continued)**

# 9.2.1.3 Application Curves



## **Typical Application (continued)**

## 9.2.2 Application for Wired Charging

The application discussed below will cover the same requirements as the first example and will add a DC supply with a secondary charger. This solution covers using a standard DC supply or a USB port as the supply.

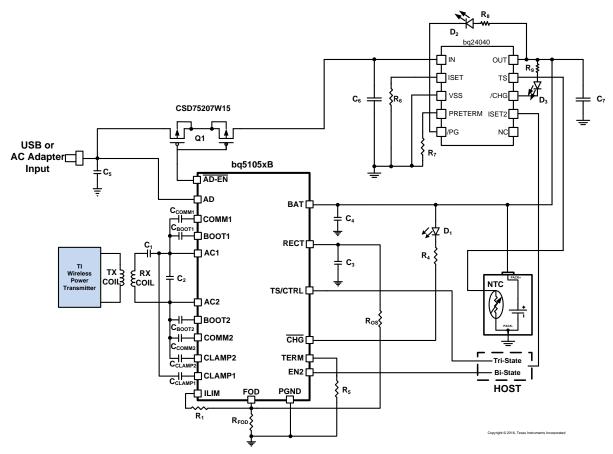


Figure 37. bq51050B Wireless Power Receiver and Wired Charger

## 9.2.2.1 Design Requirements

The requirements for this solution are identical to the first application so all common components are identical. This solution adds a wired charger and a blocking back-back FET (Q1).

The addition of a wired charger is simply enabled. The AD pin on the bq5105x is tied to the input of the DC supply. When the bq5105x senses a voltage greater than  $V_{AD-Pres}$  on the AD pin, the BAT pin will be disabled (high impedance). Once the BAT pin is disabled, the AD\_EN pin will transition and enable Q1. If wireless power is not present, the functionality of AD and AD\_EN remains and wired charging can take place.

## 9.2.2.2 Detailed Design Procedure

#### 9.2.2.2.1 Blocking Back-Back FET

Q1 is recommended to eliminate the potential for both wired and wireless systems to drive current to the simultaneously. The charge current and DC voltage level will set up parmerters for the blocking FET. The requirements for this system are 1 A for the wired charger and 5 V DC. The CSD75207W15 is chosen for its low RON and small size.

The wired charger in this solution is the bq24040. See the bq24040 datasheet (SLUS941) for specific component selection.



# **10** Power Supply Recommendations

The bq51050B requires a Qi-compatible transmitter as its power supply.

# 11 Layout

# 11.1 Layout Guidelines

- Keep the trace resistance as low as possible on AC1, AC2, and BAT.
- Detection and resonant capacitors need to be as close to the device as possible.
- COMM, CLAMP, and BOOT capacitors need to be placed as close to the device as possible.
- Via interconnect on PGND net is critical for appropriate signal integrity and proper thermal performance.
- High frequency bypass capacitors need to be placed close to RECT and OUT pins.
- ILIM and FOD resistors are important signal paths and the loops in those paths to PGND must be minimized.
- For the RHL package, connect the thermal pad to ground to help dissipate heat.

Signal and sensing traces are the most sensitive to noise; the sensing signal amplitudes are usually measured in mV, which is comparable to the noise amplitude. Make sure that these traces are not being interfered by the noisy and power traces. AC1, AC2, BOOT1, BOOT2, COMM1, and COMM2 are the main source of noise in the board. These traces should be shielded from other components in the board. It is usually preferred to have a ground copper area placed underneath these traces to provide additional shielding. Also, make sure they do not interfere with the signal and sensing traces. The PCB should have a ground plane (return) connected directly to the return of all components through vias (two vias per capacitor for power-stage capacitors, one via per capacitor for small-signal components).

For a 1-A fast charge current application, the current rating for each net is as follows:

- AC1 = AC2 = 1.2 A
- OUT = 1 A
- RECT = 100 mA (RMS)
- COMMx = 300 mA
- CLAMPx = 500 mA
- All others can be rated for 10 mA or less

# 11.2 Layout Example

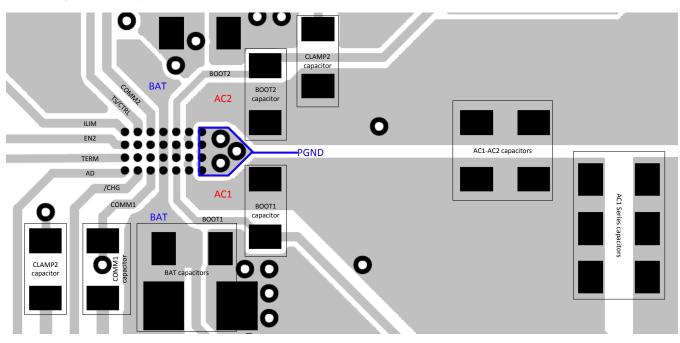


Figure 38. bq5105x Layout Example

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# **12** Device and Documentation Support

## **12.1** Documentation Support

#### 12.1.1 Related Documentation

For related documentation, see the following:

bq2404x 1A, Single-Input, Single Cell Li-Ion and Li-Pol Battery Charger With Auto Start, SLUS941

### 12.2 Related Links

The table below lists quick access links. Categories include technical documents, support and community resources, tools and software, and quick access to sample or buy.

PARTS	PRODUCT FOLDER SAMPLE & BUY TECHNICAL DOCUMENTS			TOOLS & SOFTWARE	SUPPORT & COMMUNITY
bq51050B	Click here	Click here	Click here	Click here	Click here
bq51051B	Click here	Click here	Click here	Click here	Click here
bq51052B	Click here	Click here	Click here	Click here	Click here

#### Table 2. Related Links

#### 12.3 Trademarks

All trademarks are the property of their respective owners.

#### **12.4 Electrostatic Discharge Caution**



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

## 12.5 Glossary

#### SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

## 13 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.



18-Mar-2015

# PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Device Marking (4/5)	Samples
BQ51050BRHLR	ACTIVE	VQFN	RHL	20	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR		BQ51050B	Samples
BQ51050BRHLT	ACTIVE	VQFN	RHL	20	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR		BQ51050B	Samples
BQ51050BYFPR	ACTIVE	DSBGA	YFP	28	3000	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM		BQ51050B	Samples
BQ51050BYFPT	ACTIVE	DSBGA	YFP	28	250	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM		BQ51050B	Samples
BQ51051BRHLR	ACTIVE	VQFN	RHL	20	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR		BQ51051B	Samples
BQ51051BRHLT	ACTIVE	VQFN	RHL	20	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR		BQ51051B	Samples
BQ51051BYFPR	ACTIVE	DSBGA	YFP	28	3000	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM		BQ51051B	Samples
BQ51051BYFPT	ACTIVE	DSBGA	YFP	28	250	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM		BQ51051B	Samples
BQ51052BYFPR	ACTIVE	DSBGA	YFP	28	3000	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM	0 to 125	BQ51052B	Samples
BQ51052BYFPT	ACTIVE	DSBGA	YFP	28	250	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM	0 to 125	BQ51052B	Samples

<sup>(1)</sup> The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)



18-Mar-2015

<sup>(3)</sup> MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

<sup>(4)</sup> There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

<sup>(5)</sup> Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

<sup>(6)</sup> Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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# PACKAGE MATERIALS INFORMATION

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# TAPE AND REEL INFORMATION





# QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal												
Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
BQ51050BRHLR	VQFN	RHL	20	3000	330.0	12.4	3.71	4.71	1.1	8.0	12.0	Q1
BQ51050BRHLT	VQFN	RHL	20	250	180.0	12.4	3.71	4.71	1.1	8.0	12.0	Q1
BQ51050BYFPR	DSBGA	YFP	28	3000	180.0	8.4	2.0	3.13	0.6	4.0	8.0	Q1
BQ51050BYFPT	DSBGA	YFP	28	250	180.0	8.4	2.0	3.13	0.6	4.0	8.0	Q1
BQ51051BRHLR	VQFN	RHL	20	3000	330.0	12.4	3.71	4.71	1.1	8.0	12.0	Q1
BQ51051BRHLT	VQFN	RHL	20	250	180.0	12.4	3.71	4.71	1.1	8.0	12.0	Q1
BQ51051BYFPR	DSBGA	YFP	28	3000	180.0	8.4	2.0	3.13	0.6	4.0	8.0	Q1
BQ51051BYFPT	DSBGA	YFP	28	250	180.0	8.4	2.0	3.13	0.6	4.0	8.0	Q1
BQ51052BYFPR	DSBGA	YFP	28	3000	180.0	8.4	2.0	3.13	0.6	4.0	8.0	Q1
BQ51052BYFPT	DSBGA	YFP	28	250	180.0	8.4	2.0	3.13	0.6	4.0	8.0	Q1

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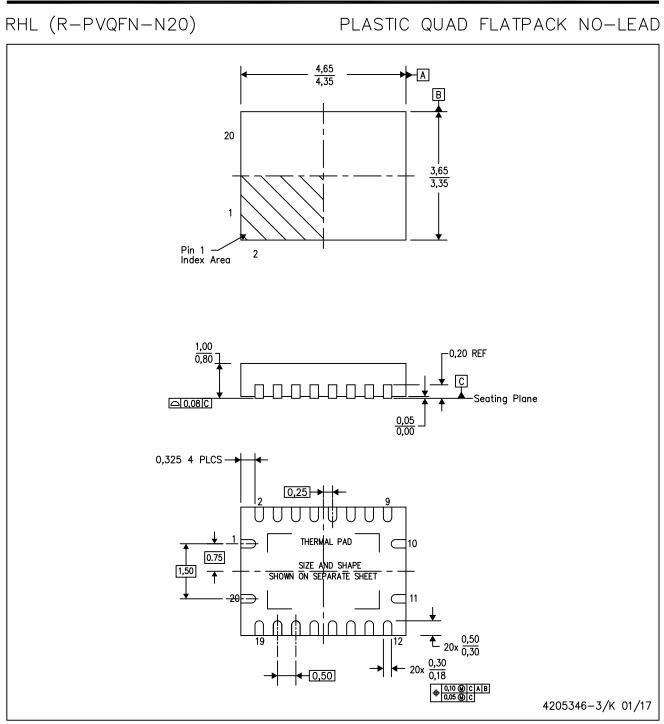
www.ti.com

# PACKAGE MATERIALS INFORMATION

17-Jun-2015



*All dimensions are nominal							
Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
BQ51050BRHLR	VQFN	RHL	20	3000	367.0	367.0	35.0
BQ51050BRHLT	VQFN	RHL	20	250	210.0	185.0	35.0
BQ51050BYFPR	DSBGA	YFP	28	3000	182.0	182.0	20.0
BQ51050BYFPT	DSBGA	YFP	28	250	182.0	182.0	20.0
BQ51051BRHLR	VQFN	RHL	20	3000	367.0	367.0	35.0
BQ51051BRHLT	VQFN	RHL	20	250	210.0	185.0	35.0
BQ51051BYFPR	DSBGA	YFP	28	3000	182.0	182.0	20.0
BQ51051BYFPT	DSBGA	YFP	28	250	182.0	182.0	20.0
BQ51052BYFPR	DSBGA	YFP	28	3000	182.0	182.0	20.0
BQ51052BYFPT	DSBGA	YFP	28	250	182.0	182.0	20.0

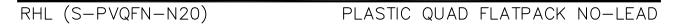


NOTES:

A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.

- B. This drawing is subject to change without notice.
- C. QFN (Quad Flatpack No-Lead) Package configuration.
- D. The package thermal pad must be soldered to the board for thermal and mechanical performance.
- E. See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions.



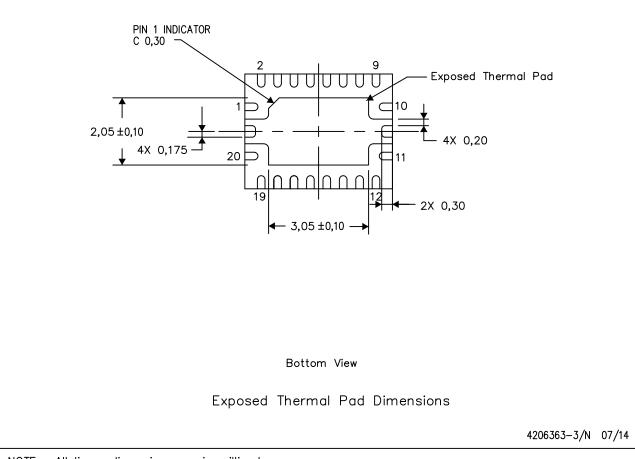


## THERMAL INFORMATION

This package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. The thermal pad must be soldered directly to the printed circuit board (PCB). After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

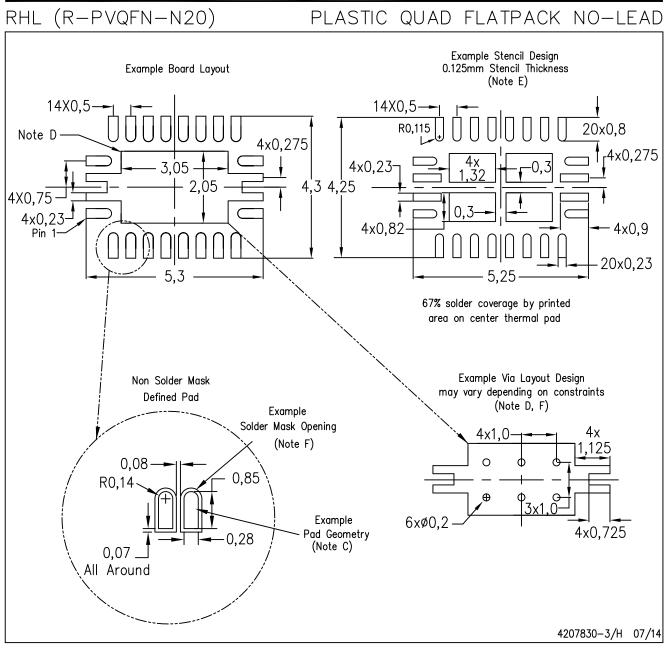
For information on the Quad Flatpack No-Lead (QFN) package and its advantages, refer to Application Report, QFN/SON PCB Attachment, Texas Instruments Literature No. SLUA271. This document is available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.







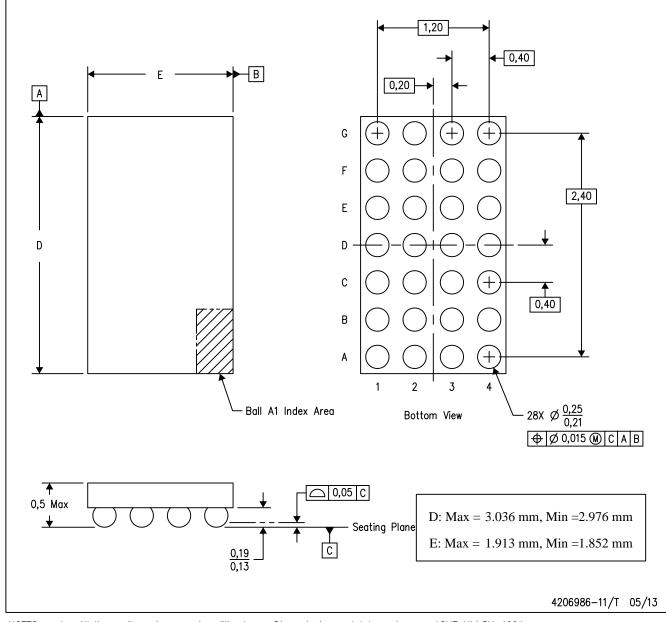


- NOTES: A. All linear dimensions are in millimeters.
  - B. This drawing is subject to change without notice.
  - C. Publication IPC-7351 is recommended for alternate designs.
  - D. This package is designed to be soldered to a thermal pad on the board. Refer to Application Note, Quad Flat-Pack Packages, Texas Instruments Literature No. SLUA271, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <a href="http://www.ti.com">http://www.ti.com</a>.
  - E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC 7525 for stencil design considerations.
  - F. Customers should contact their board fabrication site for minimum solder mask web tolerances between signal pads.



YFP (R-XBGA-N28)

DIE-SIZE BALL GRID ARRAY



NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.

B. This drawing is subject to change without notice.

C. NanoFree™ package configuration.

NanoFree is a trademark of Texas Instruments



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