

Sample &

Buy





SNVS280H-APRIL 2004-REVISED DECEMBER 2016

Support &

Community

20

LM5008 High-Voltage, 100-V Step-Down Switching Regulator

Technical

Documents

1 Features

- Integrated 100-V, N-Channel Buck Switch
- Internal V_{CC} Regulator
- No Loop Compensation Required
- Ultra-Fast Transient Response
- On-Time Varies Inversely With Line Voltage
- Operating Frequency Remains Constant With Varying Line Voltage and Load Current
- Adjustable Output Voltage
- Highly Efficient Operation
- Precision Internal Reference
- Low Bias Current
- Intelligent Current Limit Protection
- Thermal Shutdown
- 8-Pin VSSOP and 8-Pin WSON-8 (4 mm × 4 mm) Packages

2 Applications

- Non-Isolated Telecommunication Buck Regulators
- Secondary High Voltage Post Regulators
- 42-V Automotive Systems

3 Description

Tools &

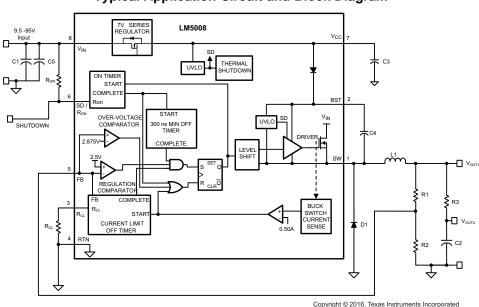
Software

The LM5008 step-down switching regulator features all of the functions needed to implement a low-cost, efficient, buck bias regulator. This high voltage regulator contains an 100-V N-channel buck switch. The device is easy to implement and is provided in the 8-pin VSSOP and the thermally enhanced 8-pin WSON packages. The regulator is based on a hysteretic control scheme using an on-time inversely proportional to V_{IN}. This feature allows the operating frequency to remain relatively constant. The hysteretic control requires no loop compensation. An intelligent current limit is implemented with forced offtime, which is inversely proportional to V_{OUT}. This scheme ensures short-circuit protection while providing minimum foldback. Other protection features include: thermal shutdown, V_{CC} undervoltage lockout, gate drive undervoltage lockout, and maximum duty cycle limiter.

Device	Informatio	n ⁽¹⁾
--------	------------	------------------

PART NUMBER	PACKAGE	BODY SIZE (NOM)
LM5008	VSSOP (8)	4.00 mm × 4.00 mm
	WSON (8)	4.00 mm × 4.00 mm

(1) For all available packages, see the orderable addendum at the end of the data sheet.



Typical Application Circuit and Block Diagram

2

Table of Contents

1	Feat	tures 1
2	Арр	lications 1
3		cription 1
4	Rev	ision History 2
5	Pin	Configuration and Functions 3
6	Spe	cifications 4
	6.1	Absolute Maximum Ratings 4
	6.2	ESD Ratings 4
	6.3	Recommended Operating Conditions 4
	6.4	Thermal Information 4
	6.5	Electrical Characteristics 5
	6.6	Switching Characteristics 5
	6.7	Typical Characteristics 6
7	Deta	ailed Description7
	7.1	Overview 7
	7.2	Functional Block Diagram 7
	7.3	Feature Description

	7.4	Device Functional Modes	11
8	Арр	lication and Implementation	12
	8.1	Application Information	12
	8.2	Typical Application	12
9	Pow	er Supply Recommendations	16
10	Lay	out	16
	10.1	Layout Guidelines	16
	10.2	Layout Examples	17
11	Dev	ice and Documentation Support	18
	11.1	Device Support	18
	11.2	Documentation Support	18
	11.3	Receiving Notification of Documentation Updates	18
	11.4	Community Resources	18
	11.5	Trademarks	18
	11.6	Electrostatic Discharge Caution	19
	11.7	Glossary	19
12		hanical, Packaging, and Orderable mation	19

4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

C	Changes from Revision G (March 2013) to Revision H P		
•	Added ESD Ratings table, Feature Description section, Device Functional Modes, Application and Implementation section, Power Supply Recommendations section, Layout section, Device and Documentation Support section, and Mechanical, Packaging, and Orderable Information section	1	
•	Deleted Lead temperature, soldering (260°C maximum)	4	
•	Changed R _{0JA} values From: 200°C/W To: 139.7°C/W (VSSOP) and From: 40°C/W To: 42°C/W (WSON)	4	

Changes from Revision F (March 2013) to Revision G

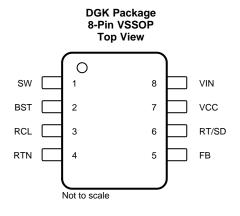
•	Changed layout of National Data Sheet to TI format
---	--

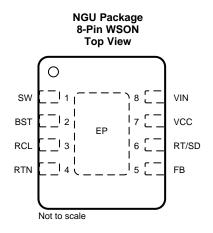
www.ti.com

Page



5 Pin Configuration and Functions





Pin Functions

	PIN	ТҮРЕ	DESCRIPTION
NO.	NAME	ITPE	DESCRIPTION
1	SW	Р	Switching node: power switching node. Connect to the output inductor, re-circulating diode, and bootstrap capacitor.
2	BST	I	Boost pin (bootstrap capacitor input): an external capacitor is required between the BST and the SW pins. A 0.01- μ F ceramic capacitor is recommended. An internal diode charges the capacitor from V _{CC} .
3	R _{CL}	I	Current limit OFF time set pin: a resistor between this pin and RTN sets the off-time when current limit is detected. The off-time is preset to 35 μ s if FB = 0 V. Toff = 10 ⁻⁵ / (0.285 + (FB / 6.35 × 10 ⁻⁶ × R _{CL}))
4	RTN	G	Ground pin: ground for the entire circuit.
5	FB	I	Feedback input from regulated output: this pin is connected to the inverting input of the internal regulation comparator. The regulation threshold is 2.5 V.
6	R _{ON} /SD	I	On-time set pin: a resistor between this pin and V _{IN} sets the switch on-time as a function of V _{IN} . The minimum recommended on-time is 400 ns at the maximum input voltage. This pin can be used for remote shutdown. Ton = $1.25 \times 10^{-10} R_{ON} / V_{IN}$
7	V _{CC}	Ρ	Output from the internal high voltage series pass regulator. Regulated at 7 V. If an auxiliary voltage is available to raise the voltage on this pin, above the regulation set point (7 V), the internal series pass regulator will shutdown, reducing the IC power dissipation. Do not exceed 14 V. This voltage provides gate drive power for the internal buck switch. An internal diode is provided between this pin and the BST pin. A local 0.1-µF decoupling capacitor is recommended. Series pass regulator is current limited to 10 mA.
8	V _{IN}	Р	Input voltage: recommended operating range is 9.5 V to 95 V.
_	EP	G	Exposed pad: the exposed pad has no electrical contact. Connect to system ground plane for reduced thermal resistance (WSON package only).

TEXAS INSTRUMENTS

www.ti.com

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

	MIN	MAX	UNIT
V _{IN} to GND	-0.3	100	V
BST to GND	-0.3	114	V
SW to GND (steady-state)		-1	V
BST to V _{CC}		100	V
BST to SW		14	V
V _{CC} to GND		14	V
All other inputs to GND	-0.3	7	V
Storage temperature, T _{stg}	-55	150	°C

(1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

6.2 ESD Ratings

			VALUE	UNIT
V _(FOD) Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾⁽²⁾	±2000		
	Charged-device model (CDM), per JEDEC specification JESD22-C101 ⁽³⁾	±750	v	

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) The human body model is a 100-pF capacitor discharged through a $1.5 \cdot k\Omega$ resistor into each pin.

(3) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

	MIN	MAX	UNIT
V _{IN}	9.5	95	V
Operating junction temperature, T_J	-40	125	°C

6.4 Thermal Information

	Junction-to-board thermal resistance Junction-to-top characterization parameter Junction-to-board characterization parameter	LM5	LM5008		
	THERMAL METRIC ⁽¹⁾	DGK (VSSOP)	NGU (WSON)	UNIT	
		8 PINS	8 PINS		
R_{\thetaJA}	Junction-to-ambient thermal resistance	139.7	42	°C/W	
R _{0JC(top)}	Junction-to-case (top) thermal resistance	51.2	27.6	°C/W	
$R_{\theta JB}$	Junction-to-board thermal resistance	70.5	18.5	°C/W	
ΨJT	Junction-to-top characterization parameter	3.4	0.3	°C/W	
Ψјв	Junction-to-board characterization parameter	69.5	18.5	°C/W	
R _{0JC(bot)}	Junction-to-case (bottom) thermal resistance	_	4.3	°C/W	

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

6.5 Electrical Characteristics

Specifications are for $T_J = 25^{\circ}C$ and $V_{IN} = 48 \text{ V}$ (unless otherwise stated)⁽¹⁾.

	PARAMETER	TEST CONE	ITIONS	MIN	TYP	MAX	UNIT
V _{CC} SUPP	LY						
		$T_J = 25^{\circ}C$			7		
V _{CC} Reg	V _{CC} regulator output	$T_J = -40^{\circ}C$ to 125°C		6.6		7.4	V
	V _{CC} current limit ⁽²⁾				9.5		mA
	V _{CC} undervoltage lockout voltage	V _{CC} increasing			6.3		V
	V _{CC} undervoltage hysteresis				200		mV
	V _{CC} UVLO delay (filter)	100-mV overdrive			10		μs
			$T_J = 25^{\circ}C$		485		
	I _{IN} operating current	Non-switching, $FB = 3 V$	$T_J = -40^{\circ}C$ to $125^{\circ}C$			675	μA
			$T_J = 25^{\circ}C$		76		
	I _{IN} shutdown current	$R_{ON}/SD = 0 V$	$T_J = -40^{\circ}C$ to $125^{\circ}C$			150	μA
CURRENT	LIMIT						
		$T_J = 25^{\circ}C$			0.51		
	Current limit threshold	$T_J = -40^{\circ}C$ to $125^{\circ}C$		0.41		0.61	A
	Current limit response time	I_{switch} overdrive = 0.1 A, time to sw	ritch off		400		ns
	OFF time generator (test 1)	FB = 0 V, R _{CL} = 100 K			35		μs
	OFF time generator (test 2)	FB = 2.3 V, R _{CL} = 100 K			2.56		μs
ON-TIME	GENERATOR			-			-
	- <i>i</i>		$T_J = 25^{\circ}C$		2.77		
	T _{ON} – 1	V _{IN} = 10 V, R _{ON} = 200 K	$T_J = -40^{\circ}C$ to $125^{\circ}C$	2.15		3.5	μs
	T 0		$T_J = 25^{\circ}C$		300		
	T _{ON} – 2	V _{IN} = 95 V, R _{ON} = 200 K	$T_J = -40^{\circ}C$ to $125^{\circ}C$	200		420	ns
			$T_J = 25^{\circ}C$		0.7		
	Remote shutdown threshold	Rising	$T_J = -40^{\circ}C$ to $125^{\circ}C$	0.4		1.05	V
	Remote shutdown hysteresis				35		mV
MINIMUM	OFF-TIME			1		1	
	Minimum off-timer	FB = 0 V			300		ns
REGULAT	TION AND OV COMPARATORS			-			-
		Internal reference, trip point for	$T_J = 25^{\circ}C$		2.5		
	FB reference threshold	switch ON	$T_J = -40^{\circ}C$ to $125^{\circ}C$	2.445		2.55	V
	FB overvoltage threshold	Trip point for switch OFF			2.875		V
	FB bias current				100		nA
HERMAL	SHUTDOWN	1					
Гsd	Thermal shutdown temperature				165		°C
	Thermal shutdown hysteresis				25		°C

(1) All electrical characteristics having room temperature limits are tested during production with T_A = T_J = 25°C. All hot and cold limits are

specified by correlating the electrical characteristics to process and temperature variations and applying statistical process control. The V_{CC} output is intended as a self bias for the internal gate drive power and control circuits. Device thermal limitations limit external (2) loading.

6.6 Switching Characteristics

over operating free-air temperature range (unless otherwise noted)

PARAMETER	TEST	r conditions	MIN	TYP	MAX	UNIT
Buck switch R _{DS(on)}	I _{TEST} = 200 mA ⁽¹⁾	$T_J = 25^{\circ}C$		1.15		0
	$I_{\text{TEST}} = 200 \text{ MA}^{17}$	$T_J = -40^{\circ}C$ to $125^{\circ}C$			2.47	Ω
Gate drive UVLO		T _J = 25°C		4.5		
	$V_{BST} - V_{SW}$ rising	$T_J = -40^{\circ}C$ to $125^{\circ}C$	3.4		5.5	v
Gate drive UVLO hysteresis				430		mV

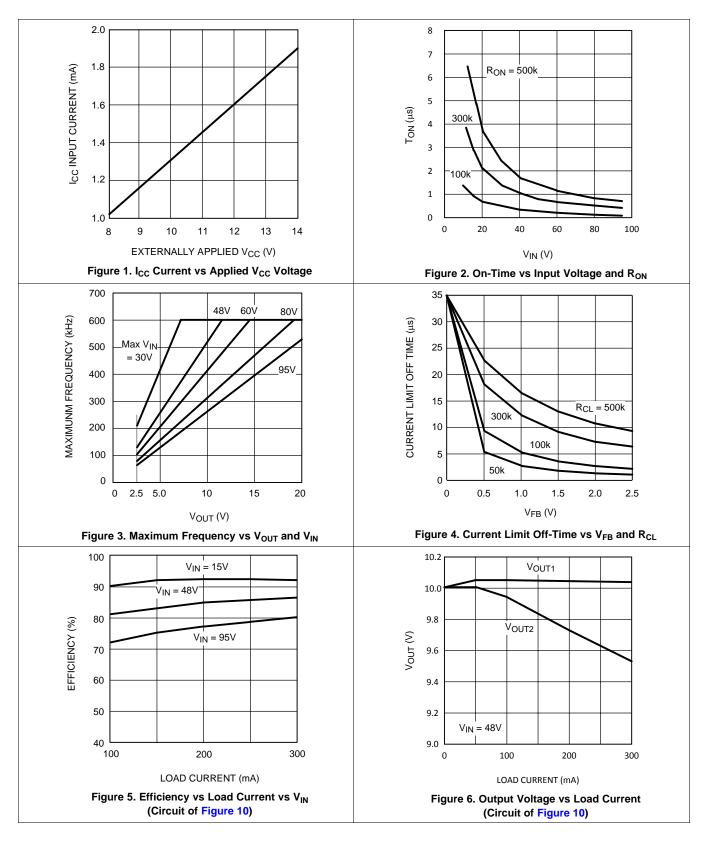
(1) For devices procured in the 8-pin WSON package the R_{DS(on)} limits are specified by design characterization data only.

LM5008 SNVS280H-APRIL 2004-REVISED DECEMBER 2016



www.ti.com

6.7 Typical Characteristics





7 Detailed Description

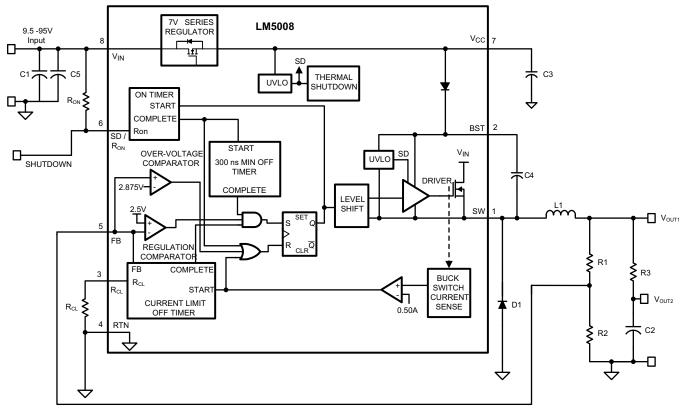
7.1 Overview

The LM5008 regulator is an easy-to-use buck DC-DC converter that operates from 9.5-V to 95-V supply voltage. The device is intended for step-down conversions from 12-V, 24-V, and 48-V unregulated, semi-regulated and fully-regulated supply rails. With integrated buck power MOSFET, the LM5008 delivers up to 350-mA DC load current with exceptional efficiency and low input quiescent current in a very small solution size.

Designed for simple implementation, a nearly fixed-frequency, constant on-time (COT) operation with discontinuous conduction mode (DCM) at light loads is ideal for low-noise, high current, fast transient load requirements. Control loop compensation is not required reducing design time and external component count.

The LM5008 incorporates other features for comprehensive system requirements, including VCC undervoltage lockout (UVLO), gate drive undervoltage lockout, maximum duty cycle limiter, intelligent current limit off timer, a precharge switch, and thermal shutdown with automatic recovery. These features enable a flexible and easy-to-use platform for a wide range of applications. The pin arrangement is designed for simple and optimized PCB layout, requiring only a few external components.

7.2 Functional Block Diagram



Copyright © 2016, Texas Instruments Incorporated

8

7.3 Feature Description

7.3.1 Hysteretic Control Circuit Overview

The LM5008 is a buck DC-DC regulator that uses a control scheme in which the on-time varies inversely with line voltage (V_{IN}). Control is based on a comparator and the on-time one-shot, with the output voltage feedback (FB) compared to an internal reference (2.5 V). If the FB level is below the reference the buck switch is turned on for a fixed time determined by the line voltage and a programming resistor (R_{ON}). Following the ON period, the switch remains off for at least the minimum off-timer period of 300 ns. If FB is still below the reference at that time, the switch turns on again for another on-time period. This will continue until regulation is achieved.

The LM5008 operates in discontinuous conduction mode at light load currents, and continuous conduction mode at heavy load current. In discontinuous conduction mode, current through the output inductor starts at zero and ramps up to a peak during the on-time, then ramps back to zero before the end of the off-time. The next on-time period starts when the voltage at FB falls below the internal reference; until then, the inductor current remains zero. In this mode the operating frequency is lower than in continuous conduction mode, and varies with load current. Therefore at light loads the conversion efficiency is maintained, because the switching losses reduce with the reduction in load and frequency. The discontinuous operating frequency can be calculated with Equation 1.

$$F = \frac{V_{OUT}^2 x L x 1.28 x 10^{20}}{R_L x (R_{ON})^2}$$

where

• R_L = the load resistance

In continuous conduction mode, current flows continuously through the inductor and never ramps down to zero. In this mode the operating frequency is greater than the discontinuous mode frequency and remains relatively constant with load and line variations. The approximate continuous mode operating frequency can be calculated with Equation 2.

$$F = \frac{V_{OUT}}{1.25 \times 10^{-10} \times R_{ON}}$$

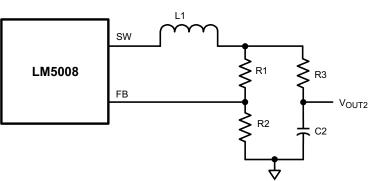
The output voltage (V_{OUT}) can be programmed by two external resistors as shown in *Functional Block Diagram*. The regulation point can be calculated with Equation 3.

$$V_{OUT} = 2.5 \times (R1 + R2) / R2$$

All hysteretic regulators regulate the output voltage based on ripple voltage at the feedback input, requiring a minimum amount of ESR for the output capacitor C2. A minimum of 25 mV to 50 mV of ripple voltage at the feedback pin (FB) is required for the LM5008. In cases where the capacitor ESR is too small, additional series resistance may be required (R3 in *Functional Block Diagram*).

For applications where lower output voltage ripple is required the output can be taken directly from a low-ESR output capacitor, as shown in Figure 7. However, R3 slightly degrades the load regulation.

Copyright © 2016, Texas Instruments Incorporated



(3)

(2)

(1)



LM5008 SNVS280H – APRIL 2004 – REVISED DECEMBER 2016

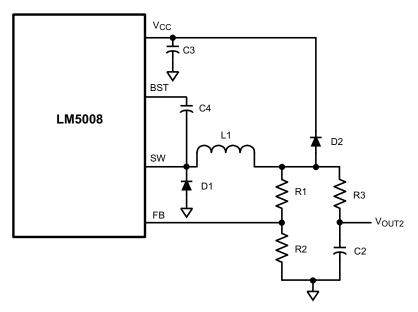
www.ti.com

Feature Description (continued)

7.3.2 High Voltage Start-Up Regulator

The LM5008 contains an internal high voltage start-up regulator. The input pin (V_{IN}) can be connected directly to the line voltages up to 95 Volts, with transient capability to 100 V. The regulator is internally current limited to 9.5 mA at V_{CC} . Upon power up, the regulator sources current into the external capacitor at V_{CC} (C3). When the voltage on the V_{CC} pin reaches the undervoltage lockout threshold of 6.3 V, the buck switch is enabled.

In applications involving a high value for V_{IN} , where power dissipation in the V_{CC} regulator is a concern, an auxiliary voltage can be diode connected to the V_{CC} pin. Setting the auxiliary voltage to 8 V to 14 V shuts off the internal regulator, reducing internal power dissipation. See Figure 8. The current required into the V_{CC} pin is shown in Figure 1.



Copyright © 2016, Texas Instruments Incorporated

Figure 8. Self-Biased Configuration

7.3.3 Regulation Comparator

The feedback voltage at FB is compared to an internal 2.5-V reference. In normal operation (the output voltage is regulated), an on-time period is initiated when the voltage at FB falls below 2.5 V. The buck switch stays on for the on-time, causing the FB voltage to rise above 2.5 V. After the on-time period, the buck switch stays off until the FB voltage again falls below 2.5 V. During start-up, the FB voltage is below 2.5 V at the end of each on-time, resulting in the minimum off-time of 300 ns. Bias current at the FB pin is nominally 100 nA.

7.3.4 Overvoltage Comparator

The feedback voltage at FB is compared to an internal 2.875-V reference. If the voltage at FB rises above 2.875 V, the on-time pulse is immediately terminated. This condition can occur if the input voltage, or the output load, change suddenly. The buck switch will not turn on again until the voltage at FB falls below 2.5 V.

7.3.5 On-Time Generator and Shutdown

The on-time for the LM5008 is determined by the R_{ON} resistor, and is inversely proportional to the input voltage (V_{IN}), resulting in a nearly constant frequency as V_{IN} is varied over its range. Equation 4 shows the on-time equation for the LM5008.

$$T_{ON} = 1.25 \times 10^{-10} \times R_{ON} / V_{IN}$$

(4)

See Figure 2. R_{ON} should be selected for a minimum on-time (at maximum V_{IN}) greater than 400 ns for proper current limit operation. This requirement limits the maximum frequency for each application, depending on V_{IN} and V_{OUT}. See Figure 3.

Feature Description (continued)

The LM5008 can be remotely disabled by taking the R_{ON} /SD pin to ground. See Figure 9. The voltage at the R_{ON} /SD pin is between 1.5 and 3 volts, depending on V_{IN} and the value of the R_{ON} resistor.

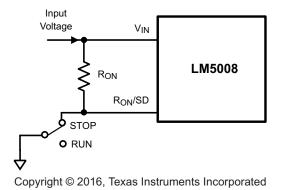


Figure 9. Shutdown Implementation

7.3.6 Current Limit

The LM5008 contains an intelligent current limit off-timer. If the current in the buck switch exceeds 0.5 A the present cycle is immediately terminated, and a non-resetable off-timer is initiated. The length of off-time is controlled by an external resistor (R_{CL}) and the FB voltage (see Figure 4). When FB = 0 V, a maximum off-time is required, and the time is preset to 35 μ s. This condition occurs when the output is shorted, and during the initial part of start-up. This amount of time ensures safe short-circuit operation up to the maximum input voltage of 95 V. In cases of overload where the FB voltage is above zero volts (not a short circuit), the current limit off-time will be less than 35 μ s. Reducing the off-time during less severe overloads reduces the amount of foldback, recovery time, and the start-up time. The off-time is calculated from Equation 5.

$$T_{OFF} = \frac{10^{-5}}{0.285 + \frac{V_{FB}}{(6.35 \times 10^{-6} \times R_{CL})}}$$

(5)

The current limit sensing circuit is blanked for the first 50-70 ns of each on-time so it is not falsely tripped by the current surge which occurs at turnon. The current surge is required by the re-circulating diode (D1) for its turnoff recovery.

7.3.7 N-Channel Buck Switch and Driver

The LM5008 integrates an N-Channel Buck switch and associated floating high voltage gate driver. The gate driver circuit works in conjunction with an external bootstrap capacitor and an internal high voltage diode. A 0.01- μ F ceramic capacitor (C4) connected between the BST pin and SW pin provides the voltage to the driver during the on-time.

During each off-time, the SW pin is at approximately 0 V, and the bootstrap capacitor charges from V_{CC} through the internal diode. The minimum off-timer, set to 300 ns, ensures a minimum time each cycle to recharge the bootstrap capacitor.

An external re-circulating diode (D1) carries the inductor current after the internal Buck switch turns off. This diode must be of the ultra-fast or Schottky type to minimize turnon losses and current overshoot.

7.3.8 Thermal Protection

The LM5008 must be operated so the junction temperature does not exceed 125°C during normal operation. An internal thermal shutdown circuit is provided to protect the LM5008 in the event of a higher than normal junction temperature. When activated, typically at 165°C, the controller is forced into a low power reset state, disabling the buck switch and the V_{CC} regulator. This feature prevents catastrophic failures from accidental device overheating. When the junction temperature reduces below 140°C (typical hysteresis = 25°C), the V_{CC} regulator is enabled, and normal operation is resumed.



7.4 Device Functional Modes

7.4.1 Shutdown Mode

(6)

The R^{ON}/SD pin provides ON and OFF control for the LM5008. When V_{SD} is below approximately 0.7 V, the device is in shutdown mode. Both the internal LDO and the switching regulator are off. The quiescent current in shutdown mode drops to 76 μ A (typical) at V_{IN} = 48 V. The LM5008 also employs VCC bias rail undervoltage protection. If the V_{CC} bias supply voltage is below its UV threshold, the regulator remains off.

7.4.2 Active Mode

LM5008 is in active mode when the internal bias rail, VCC, is above its UV threshold. Depending on the load current, the device operates in either DCM or CCM mode.

Whenever the load current is reduced to a level less than half the peak-to-peak inductor ripple current, the device enters discontinuous conduction mode (DCM). Calculate the critical conduction boundary using Equation 6.

$$I_{\text{BOUNDARY}} = \frac{\Delta I_{\text{L}}}{2} = \frac{V_{\text{OUT}} \cdot (1 - D)}{2 \cdot L_{\text{F}} \cdot F_{\text{SW}}}$$

When the inductor current reaches zero, the SW node becomes high impedance. Resonant ringing occurs at SW as a result of the LC tank circuit formed by the buck inductor and the parasitic capacitance at the SW node. At light loads, several pulses may be skipped in between switching cycles, effectively reducing the switching frequency and further improving light-load efficiency.



8 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

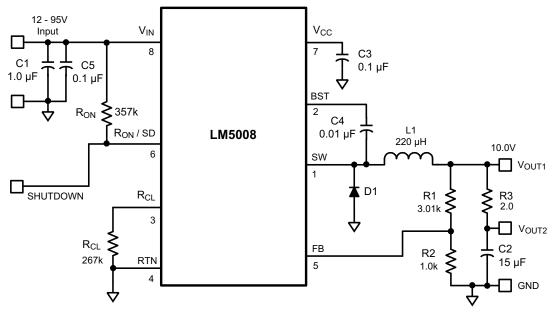
8.1 Application Information

The final circuit is shown in Figure 10. The circuit was tested, and the resulting performance is shown in Figure 12 through Figure 6.

8.1.1 Minimum Load Current

A minimum load current of 1 mA is required to maintain proper operation. If the load current falls below that level, the bootstrap capacitor may discharge during the long off-time, and the circuit will either shutdown or cycle on and off at a low frequency. If the load current is expected to drop below 1 mA in the application, the feedback resistors should be chosen low enough in value so they provide the minimum required current at nominal V_{OUT}.

8.2 Typical Application



Copyright © 2016, Texas Instruments Incorporated

Figure 10. LM5008 Example Circuit

8.2.1 Design Requirements

A guide for determining the component values will be illustrated with a design example. Table 1 lists the bill of materials for this application. The following steps will configure the LM5008 for:

- Input voltage range (V_{IN}): 12 V to 95 V
- Output voltage (V_{OUT1}): 10 V
- · Load current (for continuous conduction mode): 100 mA to 300 mA
- Maximum ripple at V_{OUT2}: 100 mVp-p at maximum input voltage



Typical Application (continued)

ITEM	DESCRIPTION	PART NUMBER	VALUE
C1	Ceramic Capacitor	TDK C4532X7R2A105M	1 µF, 100 V
C2	Ceramic Capacitor	TDK C4532X7R1E156M	15 µF, 25 V
C3	Ceramic Capacitor	Kemet C1206C104K5RAC	0.1 µF, 50 V
C4	Ceramic Capacitor	Kemet C1206C103K5RAC	0.01 µF, 50 V
C5	Ceramic Capacitor	TDK C3216X7R2A104M	0.1 µF, 100 V
D1	Ultra-Fast Power Diode	ON Semi MURA110T3	100 V, 1 A
L1	Power Inductor	Coilcraft DO3316-224 or	220 µH
		TDK SLF10145T-221MR65	
R1	Resistor	Vishay CRCW12063011F	3.01 kΩ
R2	Resistor	Vishay CRCW12061001F	1 kΩ
R3	Resistor	Vishay CRCW12062R00F	2 Ω
R _{ON}	Resistor	Vishay CRCW12063573F	357 kΩ
R _{CL}	Resistor	Vishay CRCW12062673F	267 kΩ
U1	Switching Regulator	Texas Instruments LM5008	

Table 1. Bill of Materials (Circuit of Figure 10)

8.2.2 Detailed Design Procedure

R1 and R2: From *Functional Block Diagram*, $V_{OUT1} = V_{FB} \times (R1 + R2) / R2$, and because $V_{FB} = 2.5$ V, the ratio of R1 to R2 calculates as 3:1. Standard values of 3.01 k Ω (R1) and 1.00 k Ω (R2) are chosen. Other values could be used as long as the 3:1 ratio is maintained. The selected values, however, provide a small amount of output loading (2.5 mA) in the event the main load is disconnected. This allows the circuit to maintain regulation until the main load is reconnected.

 F_s and R_{ON} : The recommended operating frequency range for the LM5008 is 50 kHz to 600 kHz. Unless the application requires a specific frequency, the choice of frequency is generally a compromise because it affects the size of L1 and C2, and the switching losses. The maximum allowed frequency, based on a minimum on-time of 400 ns, is calculated from Equation 7:

$$F_{MAX} = V_{OUT} / (V_{INMAX} \times 400 \text{ ns})$$

(7)

For this exercise, $F_{MAX} = 263$ kHz. From Equation 2, R_{ON} calculates to 304 k Ω . A standard value 357-k Ω resistor is used to allow for tolerances in Equation 2, resulting in a frequency of 224 kHz.

L1: The main parameter affected by the inductor is the output current ripple amplitude. The choice of inductor value therefore depends on both the minimum and maximum load currents, keeping in mind that the maximum ripple current occurs at maximum V_{IN} .

a. **Minimum load current:** To maintain continuous conduction at minimum Io (100 mA), the ripple amplitude (I_{OR}) must be less than 200 mAp-p so the lower peak of the waveform does not reach zero. L1 is calculated using Equation 8.

$$L1 = \frac{V_{OUT1} \times (V_{IN} - V_{OUT1})}{I_{OR} \times F_s \times V_{IN}}$$

(8)

At V_{IN} = 95 V, L1 (minimum) calculates to 200 µH. The next larger standard value (220 µH) is chosen and with this value I_{OR} calculates to 181 mAp-p at V_{IN} = 95 V, and 34 mAp-p at V_{IN} = 12 V.

b. **Maximum load current:** At a load current of 300 mA, the peak of the ripple waveform must not reach the minimum value of the LM5008's current limit threshold (410 mA). Therefore the ripple amplitude must be less than 220 mAp-p, which is already satisfied in Equation 8. With L1 = 220 μ H, at maximum V_{IN} and I_O, the peak of the ripple will be 391 mA. While L1 must carry this peak current without saturating or exceeding its temperature rating, it also must be capable of carrying the maximum value of the LM5008's current limit threshold (610 mA) without saturating, because the current limit is reached during start-up.

The DC resistance of the inductor should be as low as possible. For example, if the inductor's DCR is 1 Ω , the power dissipated at maximum load current is 0.09 W. While small, it is not insignificant compared to the load power of 3 W.

Copyright © 2004–2016, Texas Instruments Incorporated

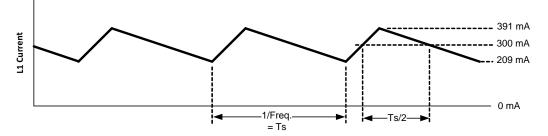


C3: The capacitor on the V_{CC} output provides not only noise filtering and stability, but its primary purpose is to prevent false triggering of the V_{CC} UVLO at the buck switch ON/OFF transitions. For this reason, C3 should be no smaller than 0.1 µF.

C2, and **R3**: When selecting the output filter capacitor C2, the items to consider are ripple voltage due to its ESR, ripple voltage due to its capacitance, and the nature of the load.

- a. ESR and R3: A low ESR for C2 is generally desirable so as to minimize power losses and heating within the capacitor. However, a hysteretic regulator requires a minimum amount of ripple voltage at the feedback input for proper loop operation. For the LM5008 the minimum ripple required at pin 5 is 25 mVp-p, requiring a minimum ripple at V_{OUT1} of 100 mV. Because the minimum ripple current (at minimum V_{IN}) is 34 mAp-p, the minimum ESR required at V_{OUT1} is 100 mV / 34 mA = 2.94 Ω . Because quality capacitors for SMPS applications have an ESR considerably less than this, R3 is inserted as shown in Functional Block Diagram. R3's value, along with C2's ESR, must result in at least 25 mVp-p ripple at pin 5. Generally, R3 will be 0.5 to 3Ω.
- b. Nature of the Load: The load can be connected to V_{OUT1} or V_{OUT2} . V_{OUT1} provides good regulation, but with a ripple voltage which ranges from 100 mV (at $V_{IN} = 12$ V) to 500 mV (at $V_{IN} = 95$ V). Alternatively, V_{OUT2} provides low ripple, but lower regulation due to R3.

For a maximum allowed ripple voltage of 100 mVp-p at V_{OUT2} (at V_{IN} = 95 V), assume an ESR of 0.4 Ω for C2. At maximum V_{IN}, the ripple current is 181 mAp-p, creating a ripple voltage of 72 mVp-p. This leaves 28 mVp-p of ripple due to the capacitance. The average current into C2 due to the ripple current is calculated using the waveform in Figure 11.





Starting when the current reaches Io (300 mA in Figure 11) half way through the on-time, the current continues to increase to the peak (391 mA), and then decreases to 300 mA half way through the off-time. The average value of this portion of the waveform is 45.5 mA, and will cause half of the voltage ripple, or 14 mV. The interval is one half of the frequency cycle time, or 2.23 µs. Using the capacitor's basic equation (see Equation 9), the minimum value for C2 is 7.2 μ F.

The ripple due to C2's capacitance is 90° out of phase from the ESR ripple, and the two numbers do not add directly. However, this calculation provides a practical minimum value for C2 based on its ESR and the target spec. To allow for the capacitor's tolerance, temperature effects, and voltage effects, a 15-µF, X7R capacitor is used.

c. In summary: The above calculations provide a minimum value for C2 and a calculation for R3. The ESR is just as important as the capacitance. The calculated values are guidelines, and should be treated as starting points. For each application, experimentation is needed to determine the optimum values for R3 and C2. (9)

$$C = I \times \Delta t / \Delta V$$

RcL: When a current limit condition is detected, the minimum off-time set by this resistor must be greater than the maximum normal off-time which occurs at maximum V_{IN}. Using Equation 4, the minimum on-time is 0.47 µs, yielding a maximum off-time of 3.99 µs. This is increased by 117 ns (to 4.11 µs) due to a ±25% tolerance of the on-time. This value is then increased to allow for:

The response time of the current limit detection loop (400 ns).

The off-time determined by Equation 5 has a $\pm 25\%$ tolerance.

 $t_{OFFCL(MIN)} = (4.11 \ \mu s + 0.40 \ \mu s) \times 1.25 = 5.64 \ \mu s$

Using Equation 5, R_{CL} calculates to 264 k Ω (at V_{FB} = 2.5 V). The closest standard value is 267 k Ω .

(10)



D1: The important parameters are reverse recovery time and forward voltage. The reverse recovery time determines how long the reverse current surge lasts each time the buck switch is turned on. The forward voltage drop is significant in the event the output is short-circuited as it is only this diode's voltage which forces the inductor current to reduce during the forced off-time. For this reason, a higher voltage is better, although that affects efficiency. A good choice is an ultra-fast power diode, such as the MURA110T3 from ON Semiconductor. Its reverse recovery time is 30 ns, and its forward voltage drop is approximately 0.72 V at 300 mA at 25°C. Other types of diodes may have a lower forward voltage drop, but may have longer recovery times, or greater reverse leakage. D1's reverse voltage rating must be at least as great as the maximum V_{IN} , and its current rating be greater than the maximum current limit threshold (610 mA).

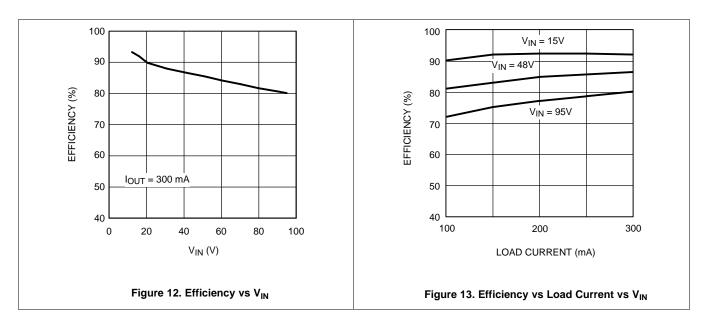
C1: This capacitor's purpose is to supply most of the switch current during the on-time, and limit the voltage ripple at V_{IN} , on the assumption that the voltage source feeding V_{IN} has an output impedance greater than zero. At maximum load current when the buck switch turns on, the current into pin 8 will suddenly increase to the lower peak of the output current waveform, ramp up to the peak value, then drop to zero at turnoff. The average input current during this on-time is the load current (300 mA). For a worst case calculation, C1 must supply this average load current during the maximum on-time. To keep the input voltage ripple to less than 2 V (for this exercise), C1 is calculated with Equation 11.

$$C1 = \frac{1 \times t_{ON}}{\Delta V} = \frac{0.3A \times 3.72 \,\mu s}{2.0V} = 0.56 \,\mu F$$
(11)

Quality ceramic capacitors in this value have a low ESR which adds only a few millivolts to the ripple. It is the capacitance which is dominant in this case. To allow for the capacitor's tolerance, temperature effects, and voltage effects, a 1.0-µF, 100-V, X7R capacitor will be used.

C4: The recommended value is 0.01 μ F for C4, as this is appropriate in the majority of applications. A highquality ceramic capacitor, with low ESR is recommended as C4 supplies the surge current to charge the buck switch gate at turnon. A low ESR also ensures a quick recharge during each off-time. At minimum V_{IN}, when the on-time is at maximum, it is possible during start-up that C4 will not fully recharge during each 300-ns off-time. The circuit will not be able to complete the start-up, and achieve output regulation. This can occur when the frequency is intended to be low (for example, R_{ON} = 500 K). In this case C4 should be increased so it can maintain sufficient voltage across the buck switch driver during each on-time.

C5: This capacitor helps avoid supply voltage transients and ringing due to long lead inductance at V_{IN} . A low-ESR, 0.1- μ F ceramic chip capacitor is recommended, placed close to the LM5008.



8.2.3 Application Curves

9 Power Supply Recommendations

The LM5008 converter is designed to operate from a wide input voltage range from 9.5 V to 95 V. The characteristics of the input supply must be compatible with the *Absolute Maximum Ratings* and *Recommended Operating Conditions*. In addition, the input supply must be capable of delivering the required input current to the fully-loaded regulator. Estimate the average input current with Equation 12.

$$I_{IN} = \frac{V_{OUT} \cdot I_{OUT}}{V_{IN} \cdot \eta}$$

where

• η is the efficiency

If the converter is connected to an input supply through long wires or PCB traces with large impedance, sachieving stable performance requires special care. The parasitic inductance and resistance of the input cables may have an adverse affect on converter operation. The parasitic inductance in combination with the low-ESR ceramic input capacitors form an underdamped resonant circuit. This circuit can cause overvoltage transients at VIN each time the input supply is cycled ON and OFF. The parasitic resistance causes the input voltage to dip during a load transient. If the regulator is operating close to the minimum input voltage, this dip can cause false UVLO fault triggering and a system reset. The best way to solve such issues is to reduce the distance from the input supply to the regulator and use an aluminum or tantalum input capacitor in parallel with the ceramics. The moderate ESR of the electrolytic capacitors helps to damp the input resonant circuit and reduce any voltage overshoots. A capacitance in the range of 10 μ F to 47 μ F is usually sufficient to provide input damping and helps to hold the input voltage steady during large load transients.

An EMI input filter is often used in front of the regulator that, unless carefully designed, can lead to instability as well as some of the effects mentioned above. The user's guide *Simple Success with Conducted EMI for DC-DC Converters* (SNVA489) provides helpful suggestions when designing an input filter for any switching regulator.

10 Layout

10.1 Layout Guidelines

The LM5008 regulation and overvoltage comparators are very fast, and as such will respond to short duration noise pulses. Layout considerations are therefore critical for optimum performance. The components at pins 1, 2, 3, 5, and 6 should be as physically close as possible to the IC, thereby minimizing noise pickup in the printedcircuit tracks. The current loop formed by D1, L1, and C2 should be as small as possible. The ground connection from C2 to C1 must be as short and direct as possible.

If the internal dissipation of the LM5008 produces excessive junction temperatures during normal operation, good use of the printed-circuit board's (PCB) ground plane can help considerably to dissipate heat. The exposed pad on the bottom of the 8-pin WSON package can be soldered to a ground plane on the PCB, and that plane should extend out from beneath the IC to help dissipate the heat. Additionally, the use of wide PCB traces, where possible, can also help conduct heat away from the IC. Judicious positioning of the PCB within the end product, along with use of any available air flow (forced or natural convection) can help reduce the junction temperatures.



10.2 Layout Examples

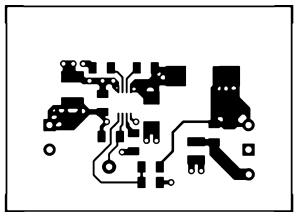


Figure 14. LM5008 Evaluation Board Top Layer

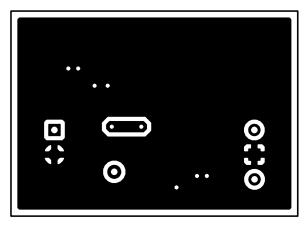
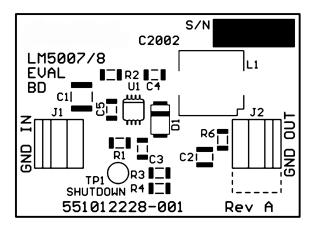
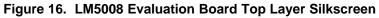


Figure 15. LM5008 Evaluation Board Bottom Layer





TEXAS INSTRUMENTS

www.ti.com

11 Device and Documentation Support

11.1 Device Support

11.1.1 Development Support

For development support see the following:

- For TI's reference design library, visit TI Designs
- For TI's WEBENCH Design Environments, visit WEBENCH[®] Design Center

11.2 Documentation Support

11.2.1 Related Documentation

For related documentation see the following:

- AN-1330 LM5008 Evaluation Board (SNVA380)
- Buck Regulator Topologies for Wide Input/Output Voltage Differentials (SNVA594)

11.2.1.1 PCB Layout Resources

- AN-1149 Layout Guidelines for Switching Power Supplies (SNVA021)
- AN-1229 Simple Switcher PCB Layout Guidelines (SNVA054)
- Constructing Your Power Supply Layout Considerations (SLUP230)
- Low Radiated EMI Layout Made SIMPLE with LM4360x and LM4600x (SNVA721)
- AN-2162 Simple Success With Conducted EMI From DC-DC Converters (SNVA489)
- Reduce Buck-Converter EMI and Voltage Stress by Minimizing Inductive Parasitics (SLYT682)

11.2.1.2 Thermal Design Resources

- AN-2020 Thermal Design By Insight, Not Hindsight (SNVA419)
- AN-1520 A Guide to Board Layout for Best Thermal Resistance for Exposed Pad Packages (SNVA183)
- Semiconductor and IC Package Thermal Metrics (SPRA953)
- Thermal Design Made Simple with LM43603 and LM43602 (SNVA719)
- PowerPAD[™]Thermally Enhanced Package (SLMA002)
- PowerPAD Made Easy (SLMA004)
- Using New Thermal Metrics (SBVA025)

11.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. In the upper right corner, click on *Alert me* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

11.4 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's Terms of Use.

TI E2E[™] Online Community *TI's Engineer-to-Engineer (E2E) Community.* Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

Design Support TI's Design Support Quickly find helpful E2E forums along with design support tools and contact information for technical support.

11.5 Trademarks

PowerPAD, E2E are trademarks of Texas Instruments. WEBENCH is a registered trademark of Texas Instruments. All other trademarks are the property of their respective owners.



11.6 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

11.7 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.



22-Feb-2016

PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package	Pins	Package	Eco Plan	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Device Marking	Samples
	(1)		Drawing		Qty	(2)	(6)	(3)		(4/5)	
LM5008MM	ACTIVE	VSSOP	DGK	8	1000	TBD	Call TI	Call TI	-40 to 125	SAYB	Samples
LM5008MM/NOPB	ACTIVE	VSSOP	DGK	8	1000	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	SAYB	Samples
LM5008MMX	NRND	VSSOP	DGK	8	3500	TBD	Call TI	Call TI	-40 to 125	SAYB	
LM5008MMX/NOPB	ACTIVE	VSSOP	DGK	8	3500	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	SAYB	Samples
LM5008SD	NRND	WSON	NGU	8	1000	TBD	Call TI	Call TI		L00040B	
LM5008SD/NOPB	NRND	WSON	NGT	8	1000	Green (RoHS & no Sb/Br)	CU NIPDAU CU SN	Level-1-260C-UNLIM		L00040B	
LM5008SDC/NOPB	ACTIVE	WSON	NGU	8	1000	Green (RoHS & no Sb/Br)	CU NIPDAU CU SN	Level-1-260C-UNLIM		L5008SD	Samples
LM5008SDCX/NOPB	ACTIVE	WSON	NGU	8	4500	Green (RoHS & no Sb/Br)	CU NIPDAU CU SN	Level-1-260C-UNLIM		L5008SD	Samples
LM5008SDX/NOPB	NRND	WSON	NGT	8	4500	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM		L00040B	

⁽¹⁾ The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

⁽³⁾ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.



22-Feb-2016

⁽⁴⁾ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

⁽⁵⁾ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

⁽⁶⁾ Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

Important Information and Disclaimer: The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

PACKAGE MATERIALS INFORMATION

www.ti.com

Texas Instruments

TAPE AND REEL INFORMATION





QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal												
Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LM5008MM	VSSOP	DGK	8	1000	178.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
LM5008MM/NOPB	VSSOP	DGK	8	1000	178.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
LM5008MMX	VSSOP	DGK	8	3500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
LM5008MMX/NOPB	VSSOP	DGK	8	3500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
LM5008SD	WSON	NGU	8	1000	178.0	12.4	4.3	4.3	1.3	8.0	12.0	Q1
LM5008SD/NOPB	WSON	NGT	8	1000	180.0	12.4	4.3	4.3	1.1	8.0	12.0	Q1
LM5008SDC/NOPB	WSON	NGU	8	1000	180.0	12.4	4.3	4.3	1.1	8.0	12.0	Q1
LM5008SDCX/NOPB	WSON	NGU	8	4500	330.0	12.4	4.3	4.3	1.1	8.0	12.0	Q1
LM5008SDX/NOPB	WSON	NGT	8	4500	330.0	12.4	4.3	4.3	1.3	8.0	12.0	Q1

Texas Instruments

www.ti.com

PACKAGE MATERIALS INFORMATION

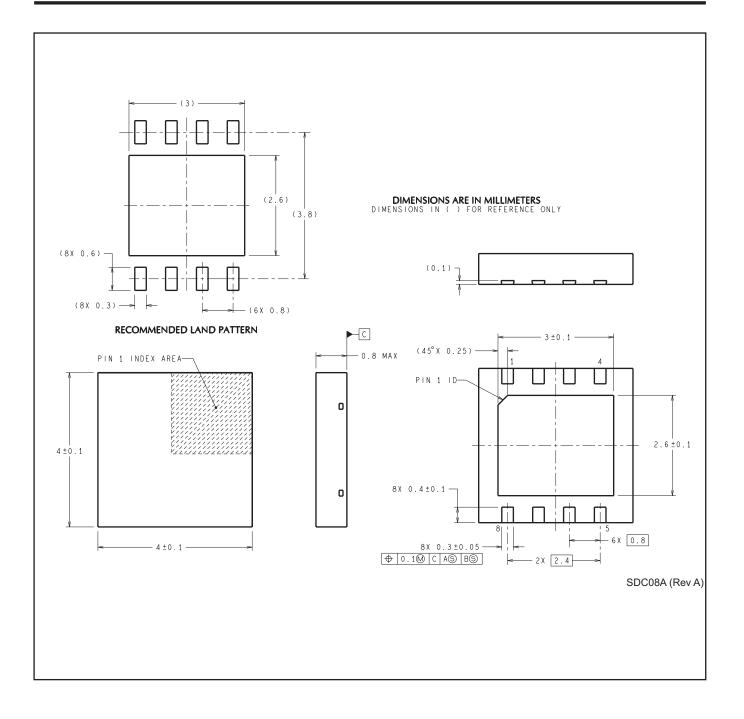
26-Aug-2016



*All dimensions are nominal							
Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LM5008MM	VSSOP	DGK	8	1000	210.0	185.0	35.0
LM5008MM/NOPB	VSSOP	DGK	8	1000	210.0	185.0	35.0
LM5008MMX	VSSOP	DGK	8	3500	367.0	367.0	35.0
LM5008MMX/NOPB	VSSOP	DGK	8	3500	367.0	367.0	35.0
LM5008SD	WSON	NGU	8	1000	210.0	185.0	35.0
LM5008SD/NOPB	WSON	NGT	8	1000	203.0	203.0	35.0
LM5008SDC/NOPB	WSON	NGU	8	1000	203.0	203.0	35.0
LM5008SDCX/NOPB	WSON	NGU	8	4500	346.0	346.0	35.0
LM5008SDX/NOPB	WSON	NGT	8	4500	367.0	367.0	35.0

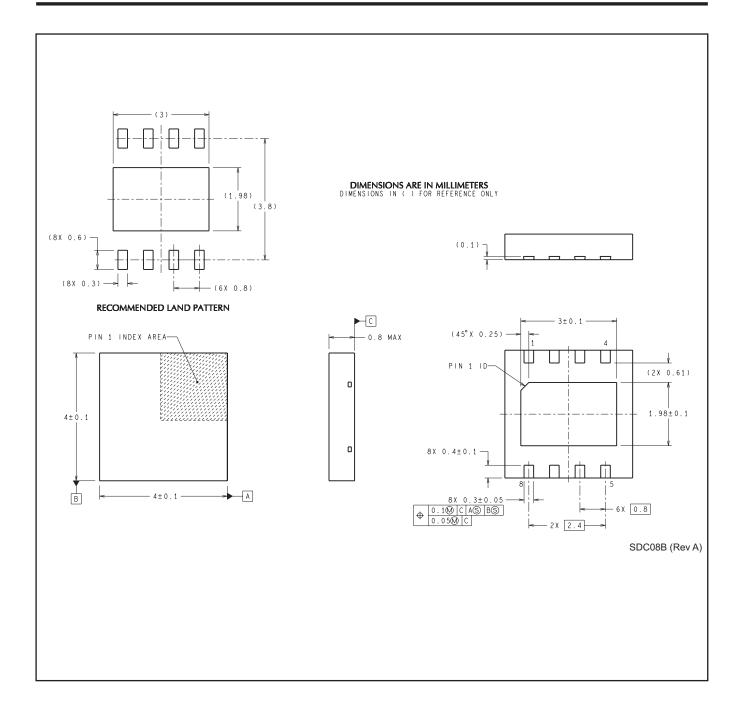
MECHANICAL DATA

NGT0008A



MECHANICAL DATA

NGU0008B



DGK (S-PDSO-G8)

PLASTIC SMALL-OUTLINE PACKAGE



NOTES: A. All linear dimensions are in millimeters.

B. This drawing is subject to change without notice.

Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 per end.

- D Body width does not include interlead flash. Interlead flash shall not exceed 0.50 per side.
- E. Falls within JEDEC MO-187 variation AA, except interlead flash.



DGK (S-PDSO-G8)

PLASTIC SMALL OUTLINE PACKAGE



NOTES: A. All linear dimensions are in millimeters.

- B. This drawing is subject to change without notice.
- C. Publication IPC-7351 is recommended for alternate designs.
- D. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
- E. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.



IMPORTANT NOTICE

Texas Instruments Incorporated and its subsidiaries (TI) reserve the right to make corrections, enhancements, improvements and other changes to its semiconductor products and services per JESD46, latest issue, and to discontinue any product or service per JESD48, latest issue. Buyers should obtain the latest relevant information before placing orders and should verify that such information is current and complete. All semiconductor products (also referred to herein as "components") are sold subject to TI's terms and conditions of sale supplied at the time of order acknowledgment.

TI warrants performance of its components to the specifications applicable at the time of sale, in accordance with the warranty in TI's terms and conditions of sale of semiconductor products. Testing and other quality control techniques are used to the extent TI deems necessary to support this warranty. Except where mandated by applicable law, testing of all parameters of each component is not necessarily performed.

TI assumes no liability for applications assistance or the design of Buyers' products. Buyers are responsible for their products and applications using TI components. To minimize the risks associated with Buyers' products and applications, Buyers should provide adequate design and operating safeguards.

TI does not warrant or represent that any license, either express or implied, is granted under any patent right, copyright, mask work right, or other intellectual property right relating to any combination, machine, or process in which TI components or services are used. Information published by TI regarding third-party products or services does not constitute a license to use such products or services or a warranty or endorsement thereof. Use of such information may require a license from a third party under the patents or other intellectual property of the third party, or a license from TI under the patents or other intellectual property of TI.

Reproduction of significant portions of TI information in TI data books or data sheets is permissible only if reproduction is without alteration and is accompanied by all associated warranties, conditions, limitations, and notices. TI is not responsible or liable for such altered documentation. Information of third parties may be subject to additional restrictions.

Resale of TI components or services with statements different from or beyond the parameters stated by TI for that component or service voids all express and any implied warranties for the associated TI component or service and is an unfair and deceptive business practice. TI is not responsible or liable for any such statements.

Buyer acknowledges and agrees that it is solely responsible for compliance with all legal, regulatory and safety-related requirements concerning its products, and any use of TI components in its applications, notwithstanding any applications-related information or support that may be provided by TI. Buyer represents and agrees that it has all the necessary expertise to create and implement safeguards which anticipate dangerous consequences of failures, monitor failures and their consequences, lessen the likelihood of failures that might cause harm and take appropriate remedial actions. Buyer will fully indemnify TI and its representatives against any damages arising out of the use of any TI components in safety-critical applications.

In some cases, TI components may be promoted specifically to facilitate safety-related applications. With such components, TI's goal is to help enable customers to design and create their own end-product solutions that meet applicable functional safety standards and requirements. Nonetheless, such components are subject to these terms.

No TI components are authorized for use in FDA Class III (or similar life-critical medical equipment) unless authorized officers of the parties have executed a special agreement specifically governing such use.

Only those TI components which TI has specifically designated as military grade or "enhanced plastic" are designed and intended for use in military/aerospace applications or environments. Buyer acknowledges and agrees that any military or aerospace use of TI components which have *not* been so designated is solely at the Buyer's risk, and that Buyer is solely responsible for compliance with all legal and regulatory requirements in connection with such use.

TI has specifically designated certain components as meeting ISO/TS16949 requirements, mainly for automotive use. In any case of use of non-designated products, TI will not be responsible for any failure to meet ISO/TS16949.

Products		Applications	
Audio	www.ti.com/audio	Automotive and Transportation	www.ti.com/automotive
Amplifiers	amplifier.ti.com	Communications and Telecom	www.ti.com/communications
Data Converters	dataconverter.ti.com	Computers and Peripherals	www.ti.com/computers
DLP® Products	www.dlp.com	Consumer Electronics	www.ti.com/consumer-apps
DSP	dsp.ti.com	Energy and Lighting	www.ti.com/energy
Clocks and Timers	www.ti.com/clocks	Industrial	www.ti.com/industrial
Interface	interface.ti.com	Medical	www.ti.com/medical
Logic	logic.ti.com	Security	www.ti.com/security
Power Mgmt	power.ti.com	Space, Avionics and Defense	www.ti.com/space-avionics-defense
Microcontrollers	microcontroller.ti.com	Video and Imaging	www.ti.com/video
RFID	www.ti-rfid.com		
OMAP Applications Processors	www.ti.com/omap	TI E2E Community	e2e.ti.com
Wireless Connectivity	www.ti.com/wirelessconne	ctivity	

Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265 Copyright © 2016, Texas Instruments Incorporated